

§ 11-3 位移法的基本体系

一、超静定结构计算的总原则：

欲求超静定结构先取一个基本体系，然后让基本体系在受力方面和变形方面与原结构完全一样。

方法的特点：

基本未知量——多余未知力；
基本体系——静定结构；
基本方程——位移条件
(变形协调条件)

位移法的特点：

基本未知量——独立结点位移
基本体系——一组单跨超静定梁
基本方程——平衡条件

二、基本未知量的选取

1、结点角位移数：

结构上可动刚结点数即为位移法计算的结点角位移数。

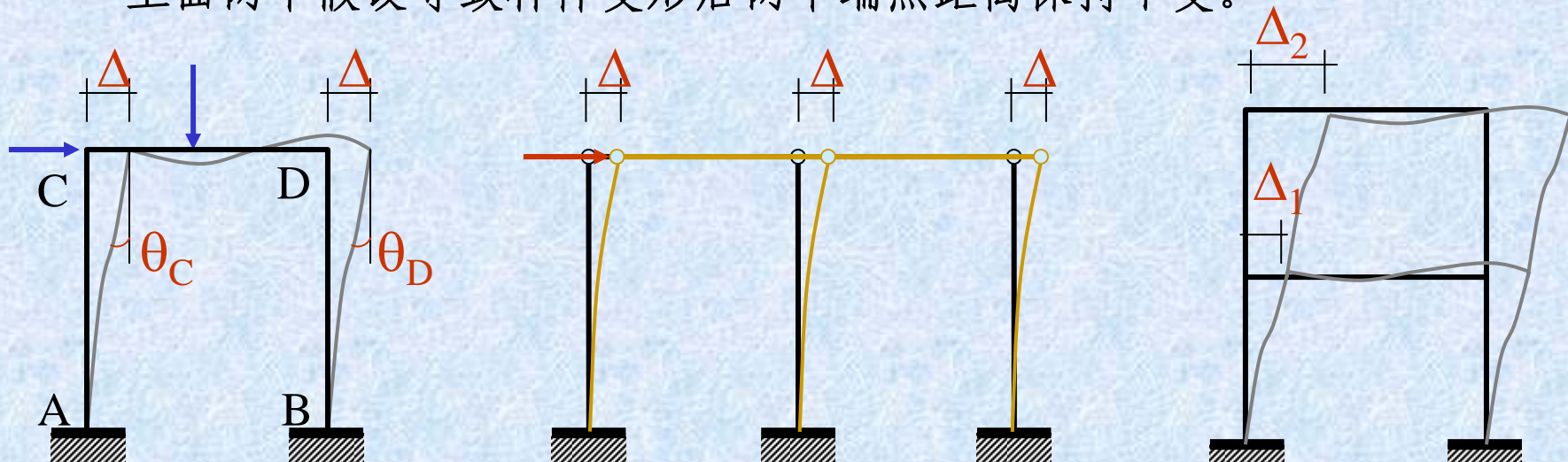
2、结构独立线位移：

每个结点有两个线位移，为了减少未知量，引入与实际相符的两个假设：

(1) 忽略轴向力产生的轴向变形——变形后的曲杆与原直杆等长；

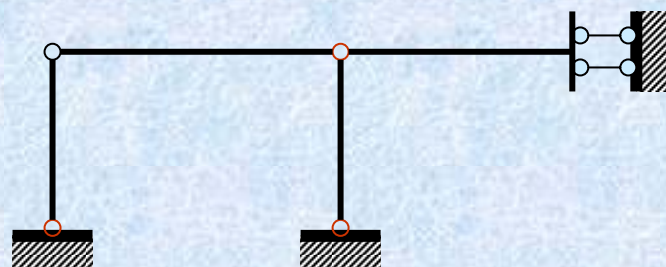
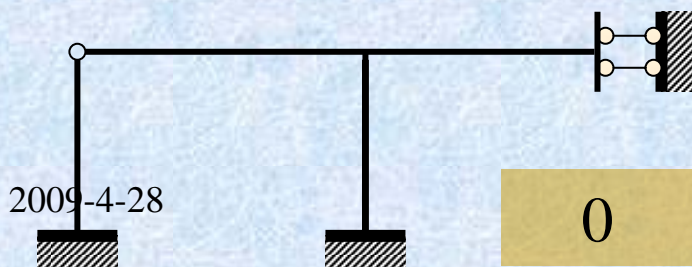
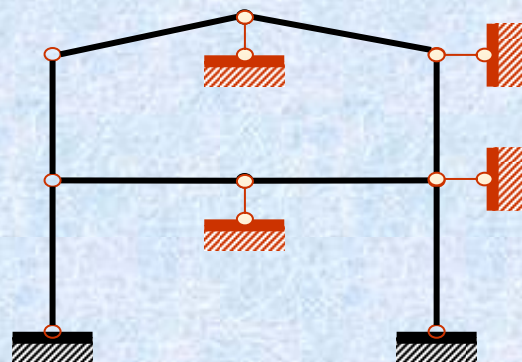
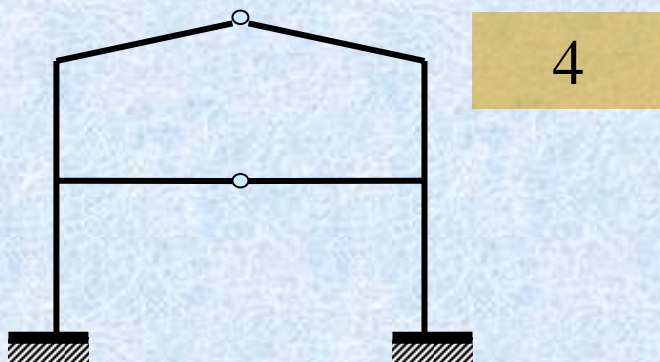
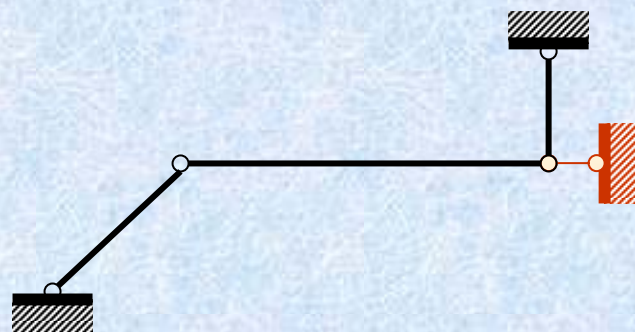
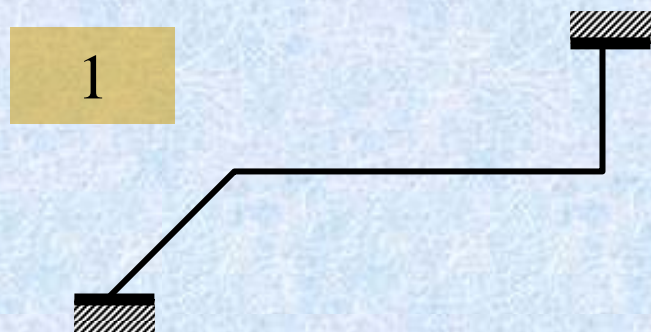
(2) 变形后的曲杆长度与其弦等长。

上面两个假设导致杆件变形后两个端点距离保持不变。

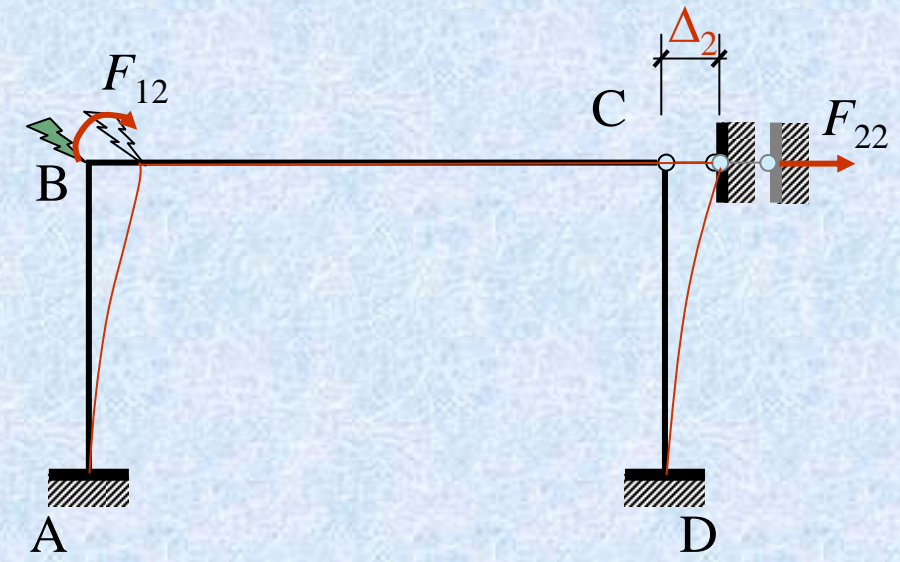
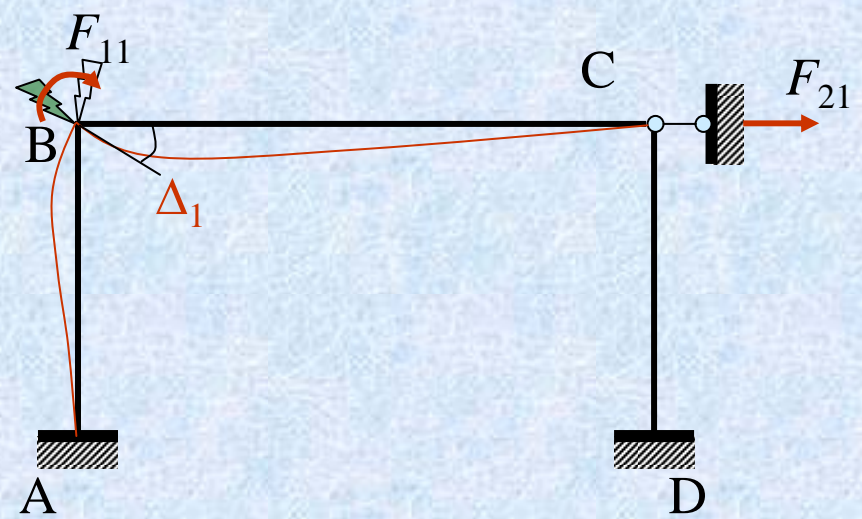
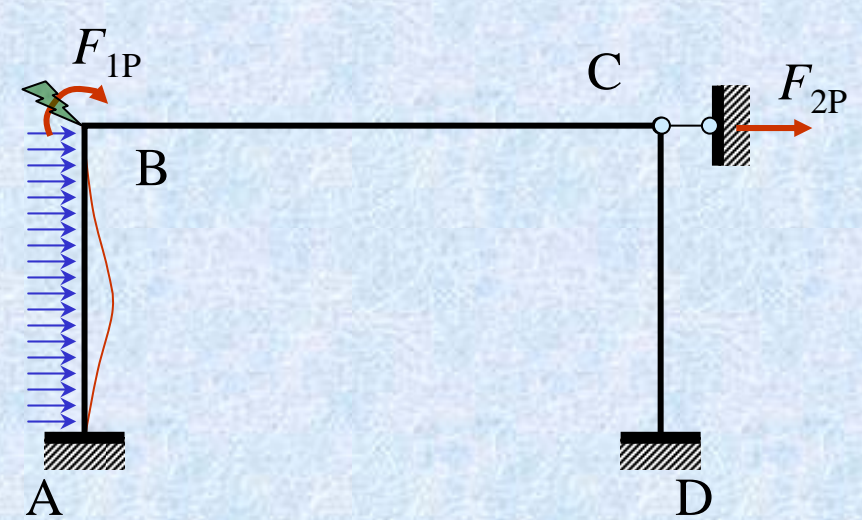
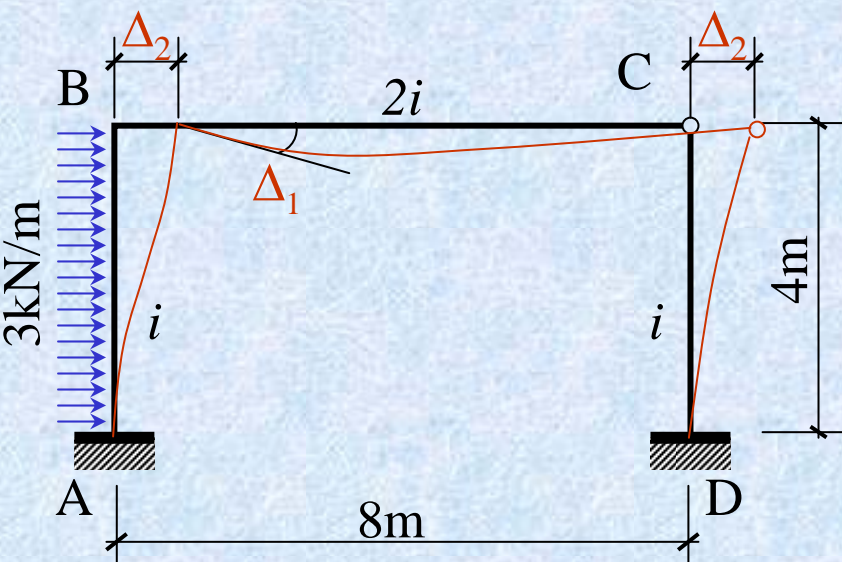


线位移数也可以用几何方法确定。

将结构中所有刚结点和固定支座，代之以铰结点和铰支座，分析新体系的几何构造性质，若为几何可变体系，则通过增加支座链杆使其变为无多余联系的几何不变体系，所需增加的链杆数，即为原结构位移法计算时的线位移数。



三、选择基本体系



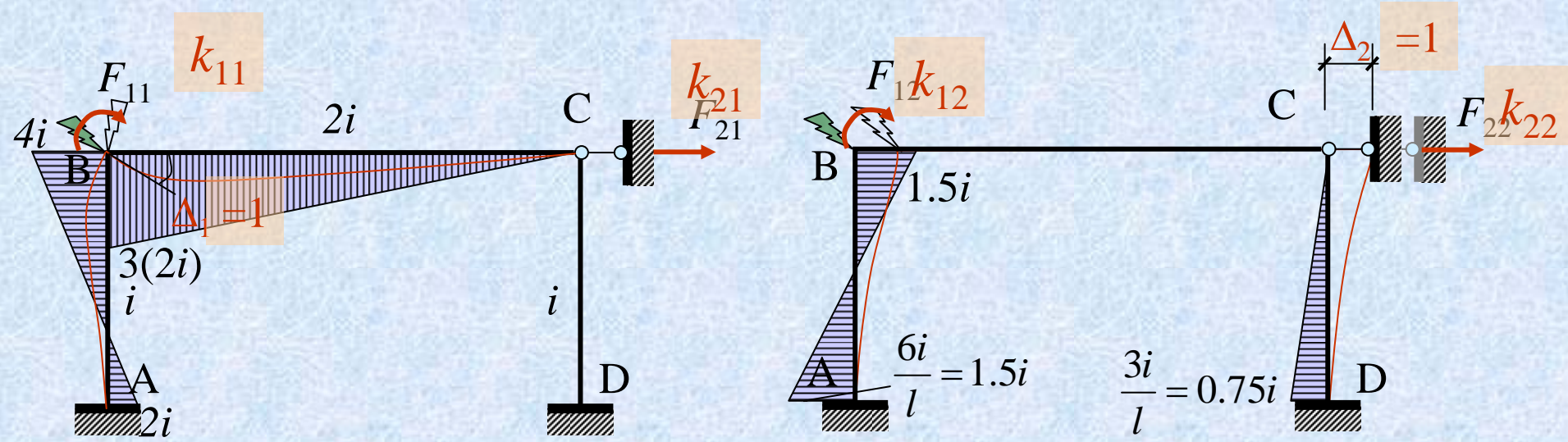
四、建立基本方程

2009-4-28

$$F_{11} + F_{12} + F_{1P} = 0 \dots \dots \dots (1a)$$

$$F_{21} + F_{22} + F_{2P} = 0 \dots \dots \dots (2a)$$



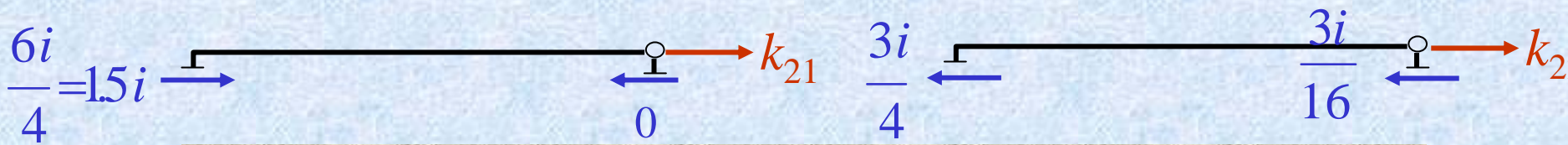
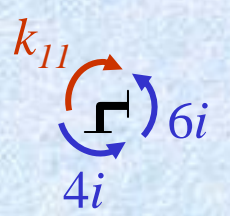


$$F_{11} + F_{12} + F_{1P} = 0 \dots \dots \dots (1a)$$

$$F_{21} + F_{22} + F_{2P} = 0 \dots \dots \dots (2a)$$

$$k_{11}\Delta_1 + k_{12}\Delta_2 + F_{1P} = 0 \dots \dots \dots (1)$$

$$k_{21}\Delta_1 + k_{22}\Delta_2 + F_{2P} = 0 \dots \dots \dots (2)$$

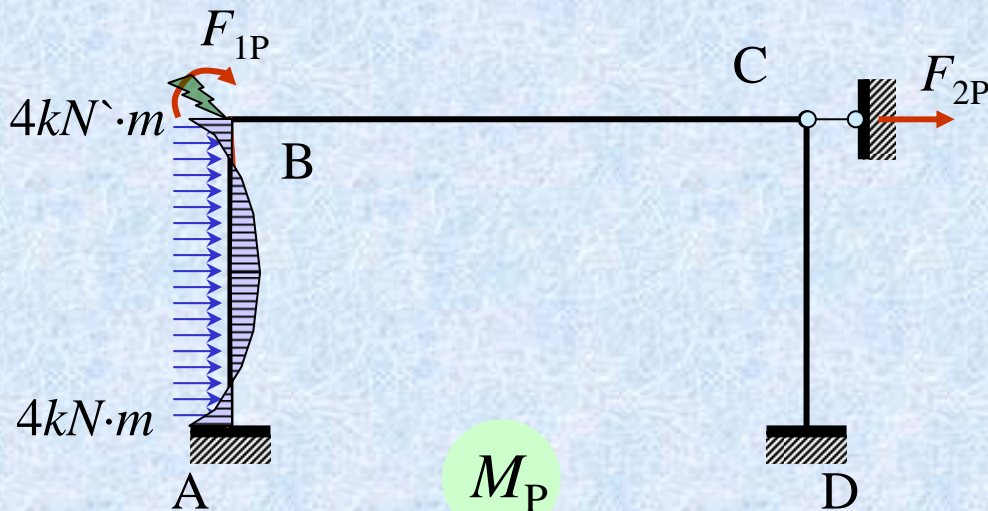


$$k_{11} = 10i \quad k_{21} = -1.5i \quad k_{12} = -1.5i \quad k_{22} = \frac{15}{16}i$$

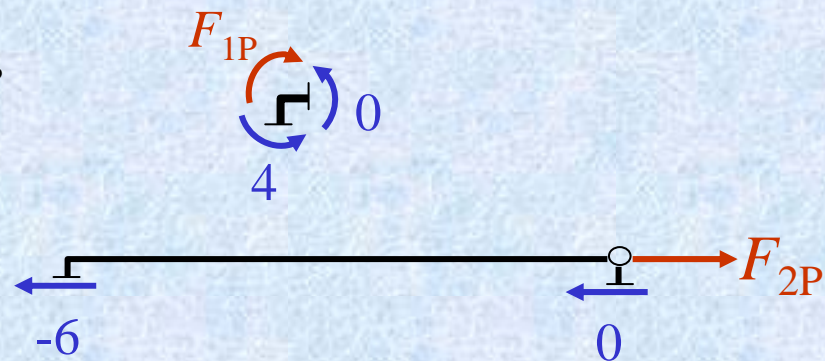
200

5





M_P



$$F_{1P} = 4 \text{ kN}\cdot\text{m} \quad F_{2P} = -6 \text{ kN}$$

位移法方程:

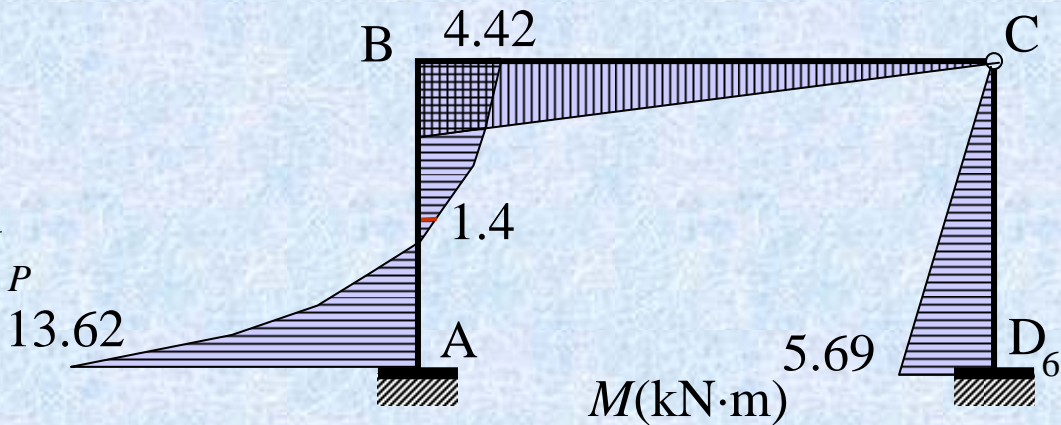
$$\left. \begin{aligned} 10 i\Delta_1 - 1.5 i\Delta_2 + 4 &= 0 \\ -1.5 i\Delta_1 + \frac{15}{16} i\Delta_2 - 6 &= 0 \end{aligned} \right\}$$

$$\Delta_1 = 0.737 \frac{1}{i} \quad \Delta_2 = 7.580 \frac{1}{i}$$

五、计算结点位移

六、绘制弯矩图

$$M = \bar{M}_1 \Delta_1 + \bar{M}_2 \Delta_2 + M_P$$

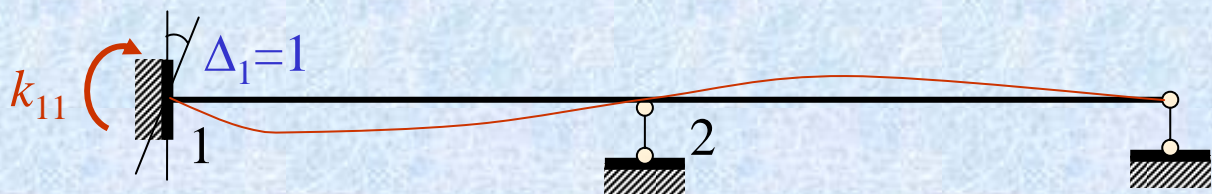


具有n个独立
结点位移的
超静定结
构:

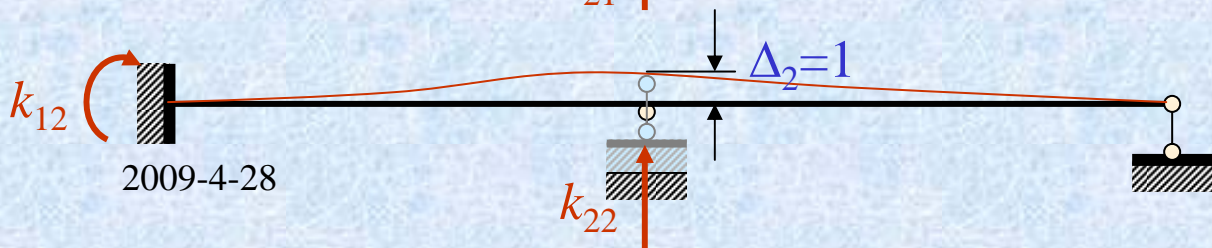
$$\left. \begin{aligned} k_{11}\Delta_1 + k_{12}\Delta_2 + \dots + k_{1n}\Delta_n + F_{1P} &= 0 \\ k_{21}\Delta_1 + k_{22}\Delta_2 + \dots + k_{2n}\Delta_n + F_{2P} &= 0 \\ \dots & \\ k_{n1}\Delta_1 + k_{n2}\Delta_2 + \dots + k_{nn}\Delta_n + F_{nP} &= 0 \end{aligned} \right\}$$

$$\begin{bmatrix} k_{11} & k_{12} & \dots & k_{1n} \\ k_{21} & k_{22} & \dots & k_{2n} \\ \dots & \dots & \dots & \dots \\ k_{n1} & k_{n2} & \dots & k_{nn} \end{bmatrix}$$

$$k_{ij} = k_{ji}$$



$$k_{11} \times 0 + k_{21} \times 1 = k_{12} \times 1 + k_{22} \times 0$$



$$k_{21} = k_{12}$$

例1、试用位移法分析图示刚架。

(1) 基本未知量

$$\Delta_1, \Delta_2, \Delta_3$$

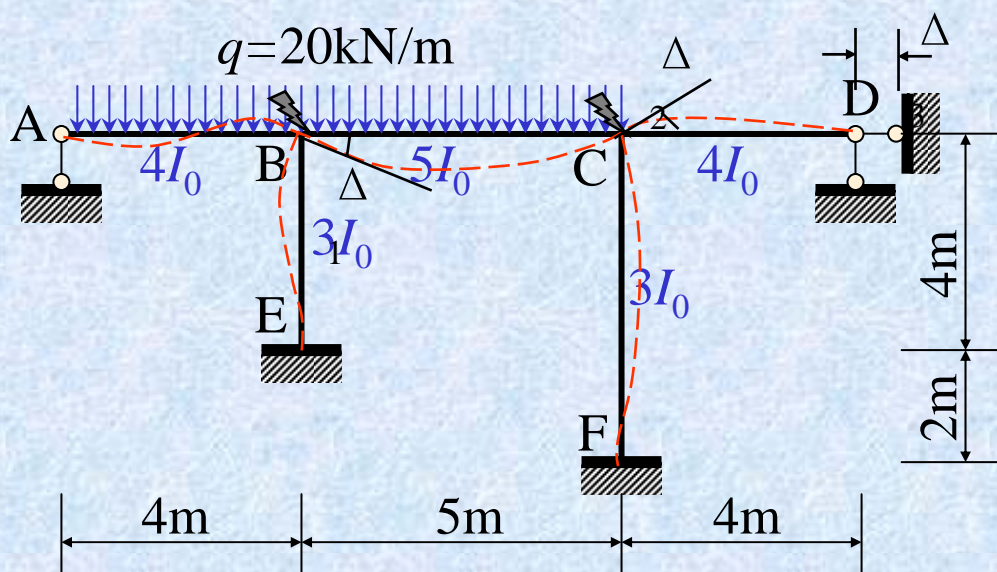
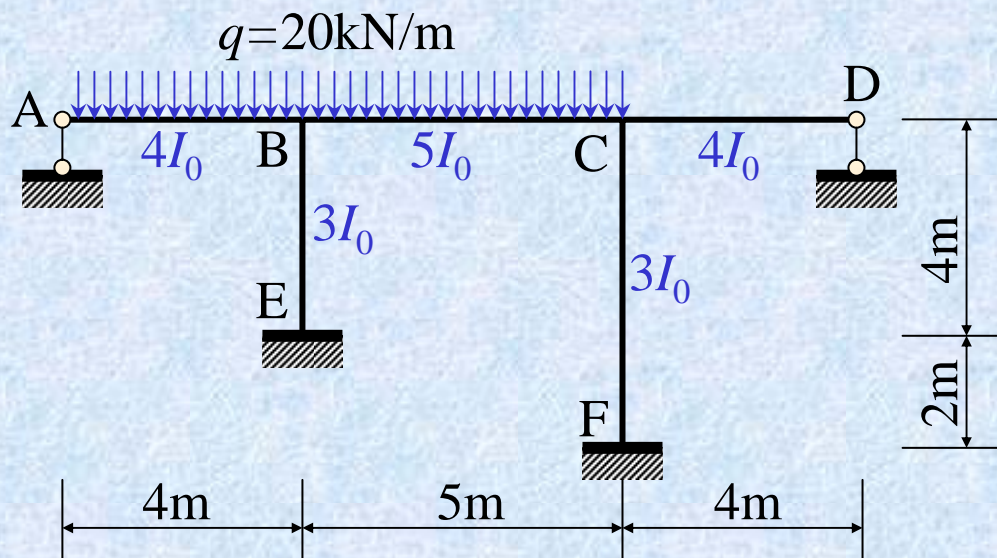
(2) 基本体系

计算杆件线性刚度*i*,
设 $EI_0=1$, 则

$$i_{AB} = \frac{EI_{AB}}{l_{AB}} = \frac{E \cdot 4I_0}{4} = 1$$

$$i_{BC} = 1, \quad i_{CD} = 1,$$

$$i_{BE} = \frac{3}{4}, \quad i_{CF} = \frac{1}{2}$$



(3) 位移法方程

$$k_{11}\Delta_1 + k_{12}\Delta_2 + k_{13}\Delta_3 + F_{1P} = 0$$

$$k_{21}\Delta_1 + k_{22}\Delta_2 + k_{23}\Delta_3 + F_{2P} = 0$$

$$k_{31}\Delta_1 + k_{32}\Delta_2 + k_{33}\Delta_3 + F_{3P} = 0$$

(4) 计算系数: k_{11} 、 k_{12} 、 k_{13} 、 k_{21} 、 k_{22} 、 k_{23} 、 k_{31} 、 k_{32} 、 k_{33}

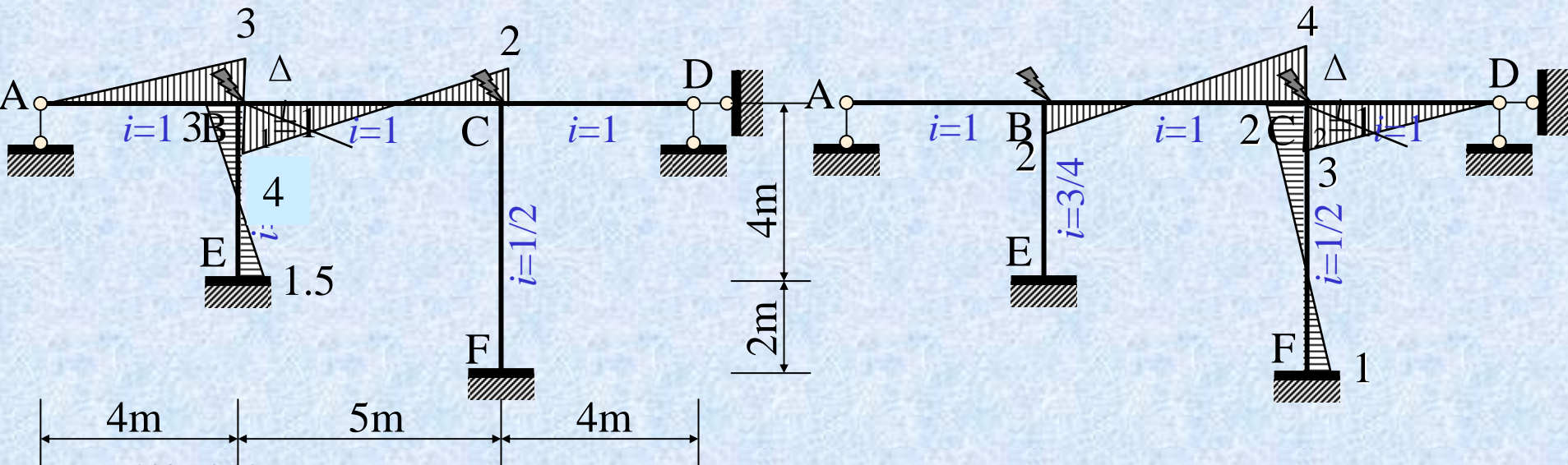
$$k_{11} = 3 + 4 + 3 = 10$$

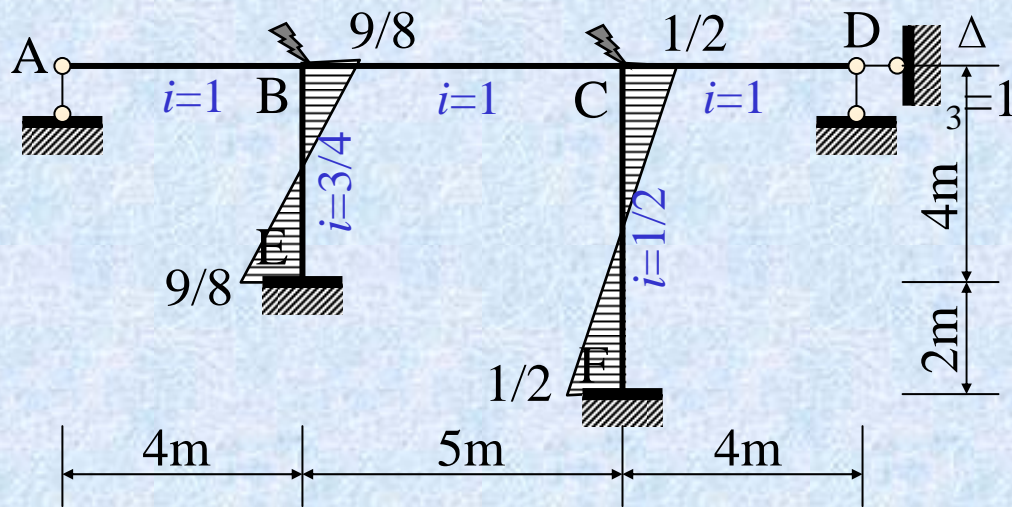
$$k_{22} = 4 + 3 + 2 = 9$$

$$k_{12} = k_{21} = 2$$

$$k_{13} = k_{31} = ?$$

$$k_{23} = k_{32} = ?$$





$$k_{33} = (1/6) + (9/16) = 35/48$$

$$k_{31} = k_{13} = -9/8$$

$$k_{32} = k_{23} = -1/2$$

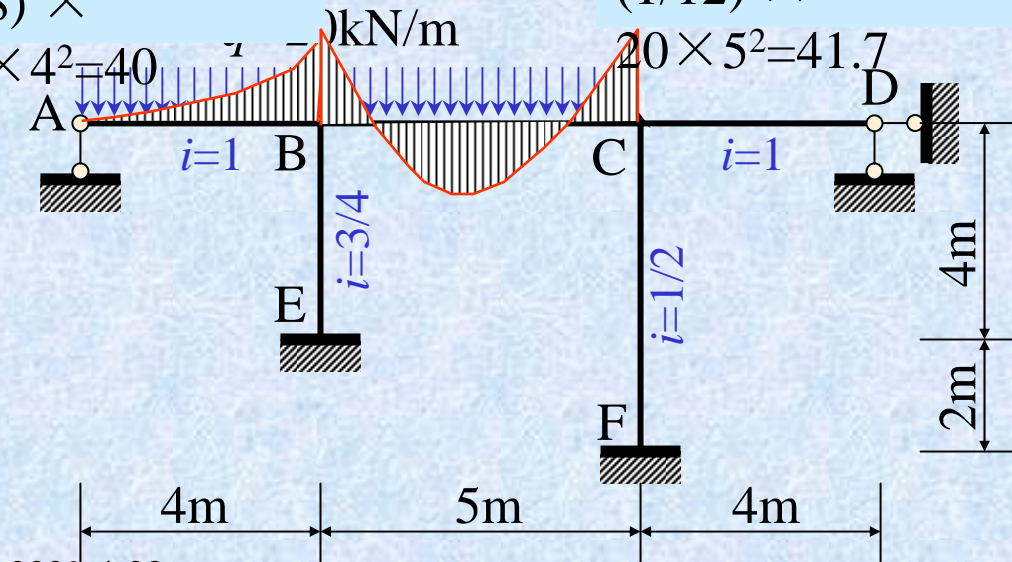
(5) 计算自由项: F_{1P} 、 F_{2P} 、 F_{3P}

$$(1/8) \times$$

$$20 \times 4^2 = 40$$

$$(1/12) \times$$

$$20 \times 5^2 = 41.7$$



$$F_{1P} = 40 - 41.7 = -1.7$$

$$F_{2P} = 41.7$$

$$F_{3P} = 0$$

(6) 建立位移法基本方程:

(7) 解方程求结点位移:

$$10\Delta_1 + 2\Delta_2 - \frac{9}{8}\Delta_3 - 1.7 = 0$$

$$\Delta_1 = 0.94$$

$$2\Delta_1 + 9\Delta_2 - \frac{1}{2}\Delta_3 + 41.7 = 0$$

$$\Delta_2 = -4.94$$

$$-\frac{9}{8}\Delta_1 - \frac{1}{2}\Delta_2 + \frac{35}{48}\Delta_3 = 0$$

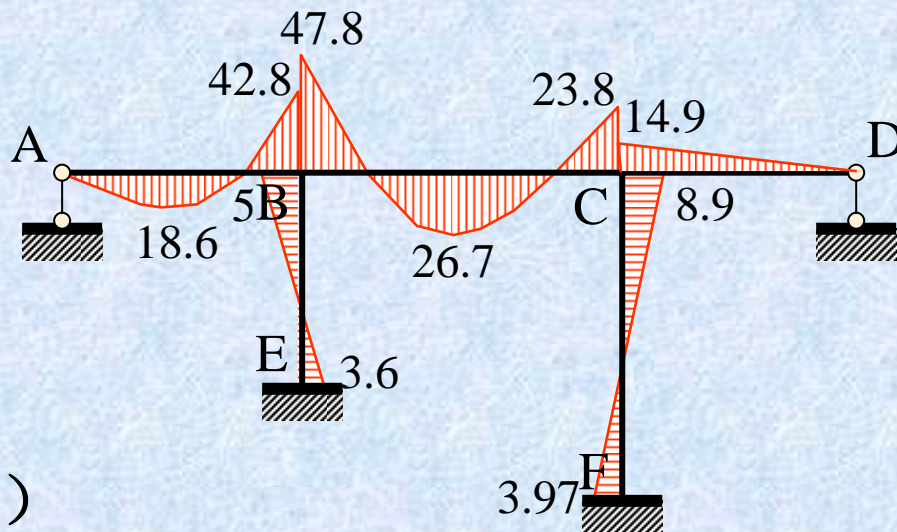
$$\Delta_3 = -1.94$$

(8) 绘制弯矩图

(9) 校核

结点及局部杆件的静力平衡条件的校核。

$$M = \overline{M}_1\Delta_1 + \overline{M}_2\Delta_2 + M_P$$

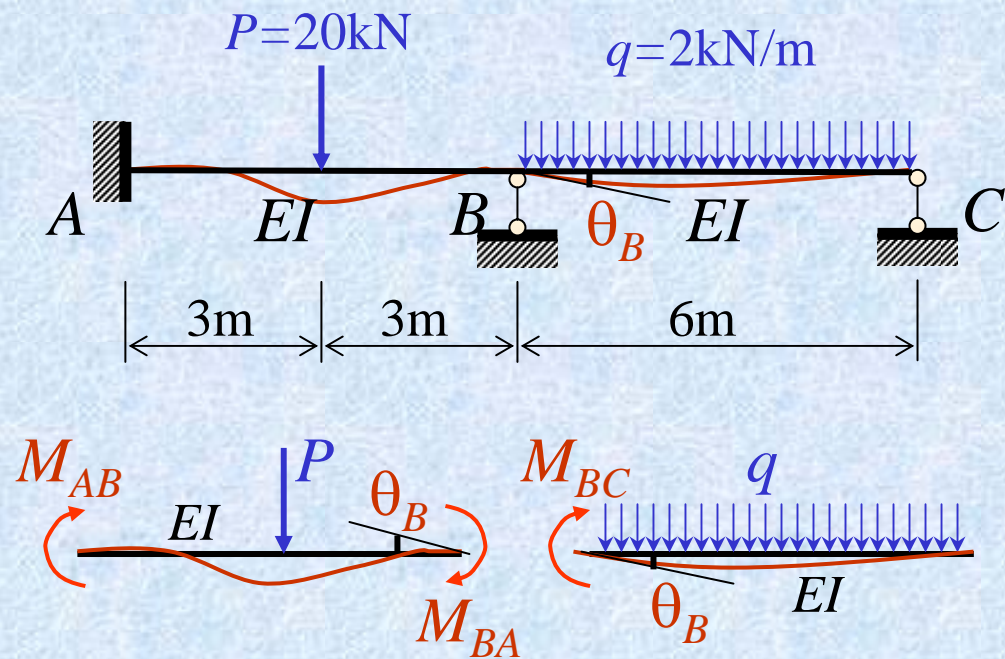


M图

(kN·m)

§ 11-4 无侧移刚架的计算

如果除支座以外，刚架的各结点只有角位移而没有线位移，这种刚架称为无侧移刚架。



1、基本未知量 θ_B

2、固端弯矩

$$m_{BA} = \frac{Pl}{8} = \frac{20 \times 6}{8} = 15 \text{ kN} \cdot \text{m}$$

$$m_{AB} = -15 \text{ kN} \cdot \text{m}$$

$$m_{BC} = -\frac{ql^2}{8} = -9 \text{ kN} \cdot \text{m}$$

3、列杆端转角位移方程

$$\text{设 } i = \frac{EI}{6} \quad M_{AB} = 2i\theta_B - 15$$

$$M_{BA} = 4i\theta_B + 15$$

$$M_{BC} = 3i\theta_B - 9$$

$$M_{BC} = 3i\theta_B - \frac{3i}{l}\Delta + m_{BC}$$

4、位移法基本方程（平衡条件）

超静定结构必须满足的三个条件:

- (1) 变形连续条件: 在确定基本未知量时得到满足;
- (2) 物理条件: 即刚度方程;
- (3) 平衡条件: 即位移法基本方程。

4、位移法基本方程 (平衡条件) 5、各杆端弯矩及弯矩图

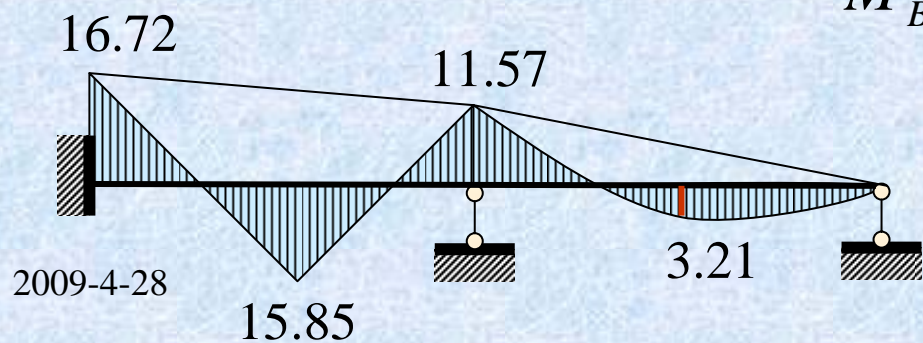
$$\sum M_B = 0 \quad M_{BA} + M_{BC} = 0 \quad M_{AB} = 2i \left(-\frac{6}{7i} \right) - 15 = -16.72 \text{ kN} \cdot \text{m}$$

$$4i\theta_B + 15 + 3i\theta_B - 9 = 0$$

$$\therefore \theta_B = -\frac{6}{7i}$$

$$M_{BA} = 4i \left(-\frac{6}{7i} \right) + 15 = 11.57 \text{ kN} \cdot \text{m}$$

$$M_{BC} = 3i \left(-\frac{6}{7i} \right) - 9 = -11.57 \text{ kN} \cdot \text{m}$$

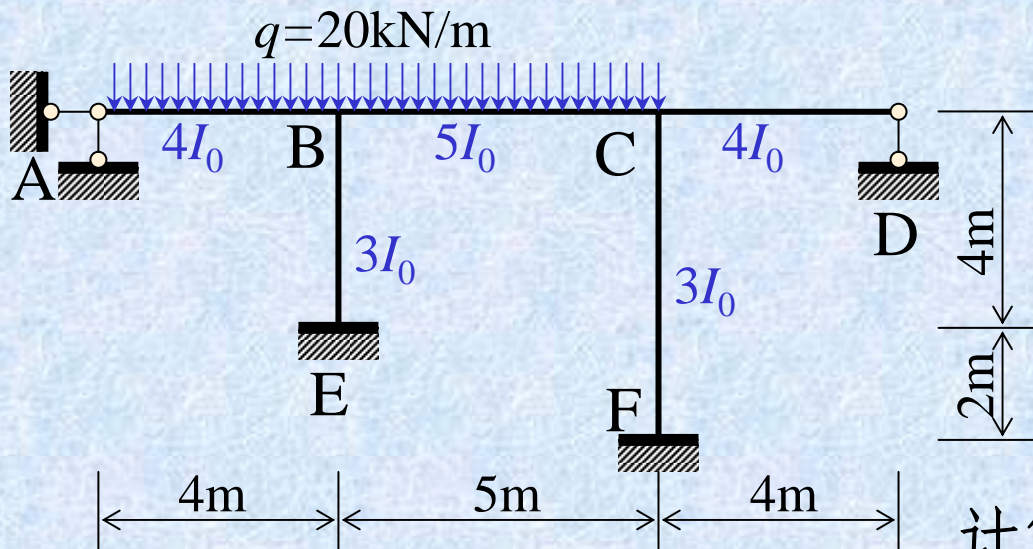


M图 (kN·m)

例1、试用位移法分析图示刚架。

(1) 基本未知量 θ_B 、 θ_C

(2) 杆端弯矩 M_{ij}



$$m_{BA} = \frac{ql^2}{8} = \frac{20 \times 4^2}{8} = 40$$

$$m_{BC} = -\frac{ql^2}{12} = -41.7$$

$$m_{CB} = 41.7$$

计算线性刚度 i ，设 $EI_0 = 1$ ，则

$$i_{AB} = \frac{EI_{AB}}{l_{AB}} = \frac{E \cdot 4I_0}{4} = 1$$

$$i_{BC} = 1, i_{CD} = 1, i_{BE} = \frac{3}{4}, i_{CF} = \frac{1}{2}$$

梁

$$M_{BA} = 3i_{AB} \cdot \theta_B + m_{BA} = 3\theta_B + 40 \quad M_{CB} = 4\theta_C + 2\theta_B + 41.7$$

$$M_{BC} = 4\theta_B + 2\theta_C - 41.7$$

$$M_{CD} = 3\theta_C$$

梁

$$M_{BA} = 3i_{AB} \cdot \theta_B + m_{BA} = 3\theta_B + 40$$

$$M_{CD} = 3\theta_C$$

$$M_{BC} = 4\theta_B + 2\theta_C - 41.7$$

$$M_{CB} = 4\theta_C + 2\theta_B + 41.7$$

柱

$$M_{BE} = 4 \cdot \frac{3}{4} \theta_B = 3\theta_B$$

$$M_{CF} = 4 \cdot \frac{1}{2} \theta_C = 2\theta_C$$

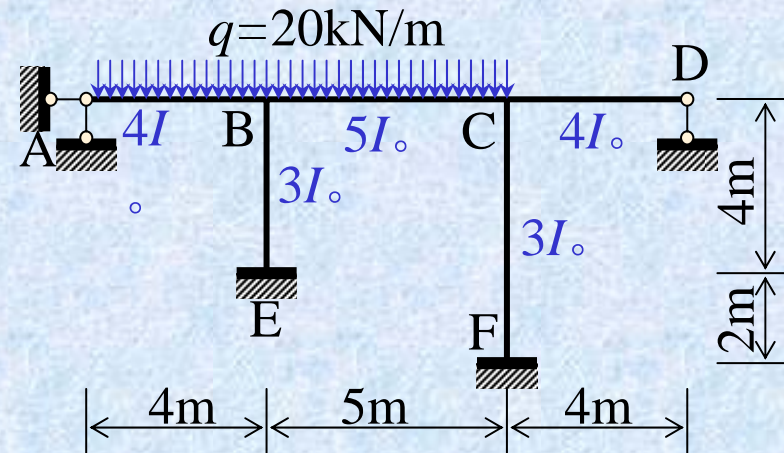
$$M_{EB} = 2 \cdot \frac{3}{4} \theta_B = 1.5\theta_B$$

$$M_{FC} = 2 \cdot \frac{1}{2} \theta_C = \theta_C$$

(3) 位移法方程

$$\left. \begin{aligned} \sum M_B = 0 \quad M_{BA} + M_{BC} + M_{BE} = 0 \\ \sum M_C = 0 \quad M_{CB} + M_{CD} + M_{CF} = 0 \end{aligned} \right\}$$

$$\left. \begin{aligned} 10\theta_B + 2\theta_C - 1.7 = 0 \\ 2\theta_B + 9\theta_C + 41.7 = 0 \end{aligned} \right\}$$



(4) 解方程

$$\theta_B = 1.15 \quad \theta_C = -4.89 \quad (\text{相对值})$$

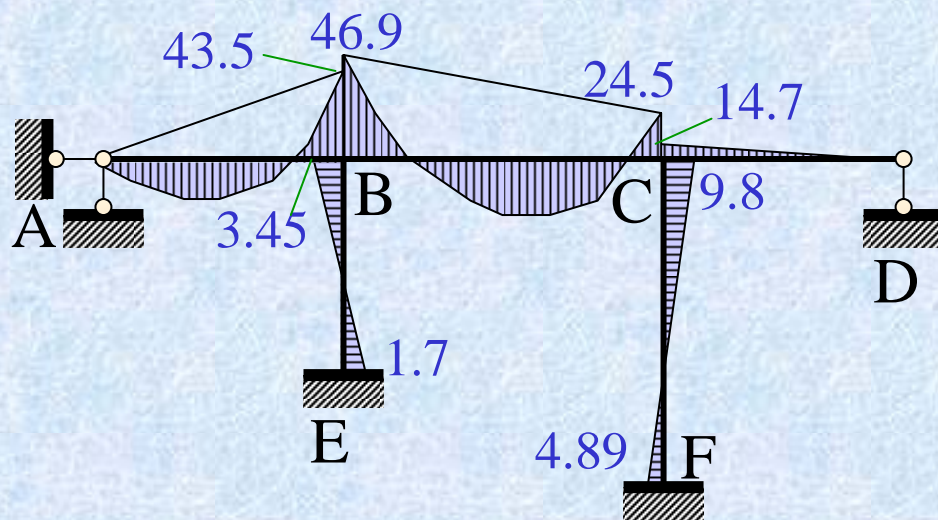
(5) 杆端弯矩及弯矩图

梁

$$\begin{cases} M_{BA} = 3i_{AB} \cdot \theta_B + m_{BA} = 3\theta_B + 40 = 3 \times 1.15 + 40 = 43.5 \text{ kN} \cdot \text{m} \\ M_{BC} = 4\theta_B + 2\theta_C - 41.7 = 4 \times 1.15 + 2 \times (-4.89) - 41.7 = -46.9 \text{ kN} \cdot \text{m} \\ \dots\dots\dots \end{cases}$$

柱

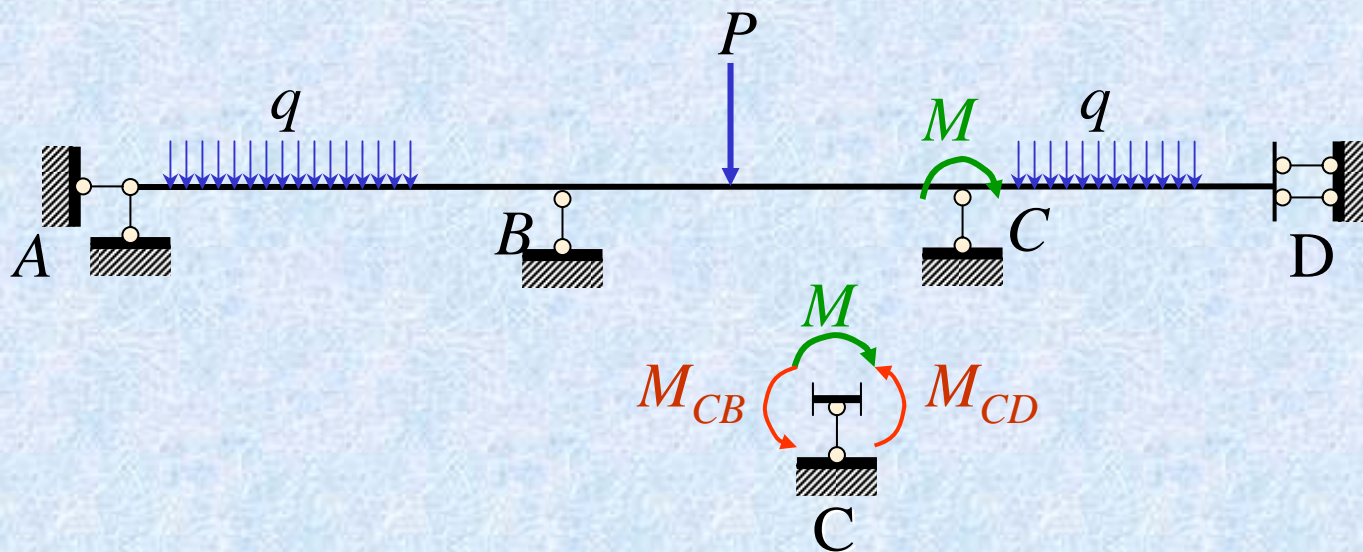
$$\begin{cases} M_{BE} = 4 \cdot \frac{3}{4} \theta_B = 3\theta_B = 3 \times 1.15 = 3.45 \text{ kN} \cdot \text{m} \\ M_{CF} = 4 \cdot \frac{1}{2} \theta_C = 2\theta_C = 2 \times (-4.89) = -9.8 \text{ kN} \cdot \text{m} \end{cases}$$



M图 (kN · m)

小结

- 1、有几个未知结点位移就应建立几个平衡方程；
- 2、单元分析、建立单元刚度方程是基础；
- 3、当结点作用有集中外力矩时，结点平衡方程式中应包括外力矩。



有侧移刚架的计算

$$M_{AB} = -\frac{3i}{l}\Delta + m_{AB} = -\frac{3i}{l} \times \frac{ql^3}{16i} - \frac{ql^2}{8} = -\frac{5ql^2}{16}$$

$$M_{CD} = -\frac{3i}{l}\Delta = -\frac{3ql^2}{16}$$

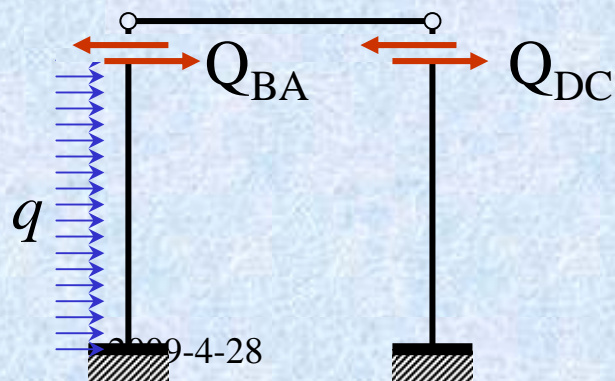
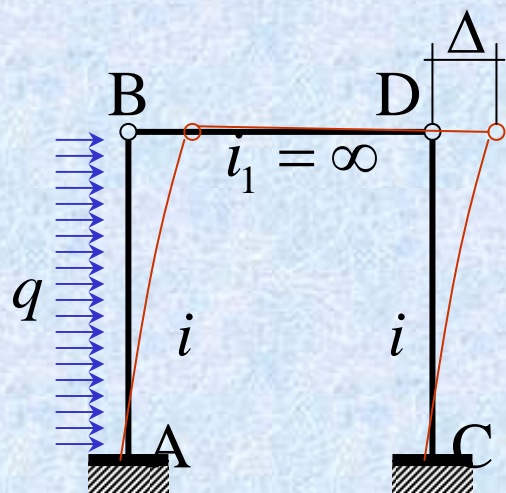
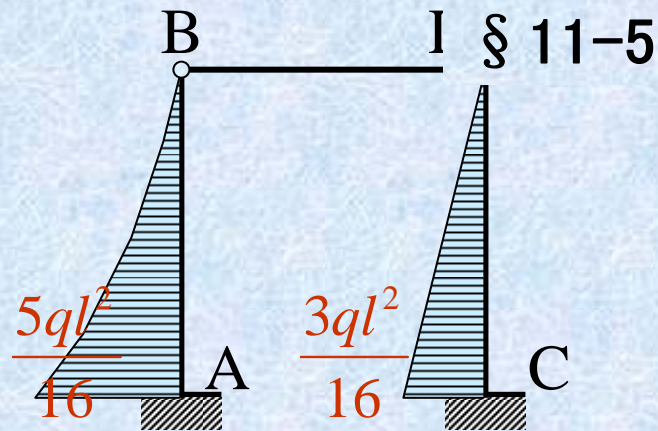
$$\sum x = 0 \quad Q_{BA} + Q_{DC} = 0$$

其中 $Q_{BA} = \frac{3i}{l^2}\Delta - \frac{3}{8}ql$ $Q_{DC} = \frac{3i}{l^2}\Delta$

$$\frac{6i}{l^2}\Delta - \frac{3}{8}ql = 0 \quad \Delta = \frac{ql^3}{16i}$$

绘制弯矩图的方法:

- (1) 直接由外荷载及剪力计算;
- (2) 由角变位移方程计算。



例：作图示刚架的弯矩图。忽略梁的轴向变形。

解：1) 基本未知量： Δ

2) 各柱的杆端剪力

侧移刚度 $J=3i/h^2$ ，则：

$$Q_1=J_1\Delta, \quad Q_2=J_2\Delta, \quad Q_3=J_3\Delta$$

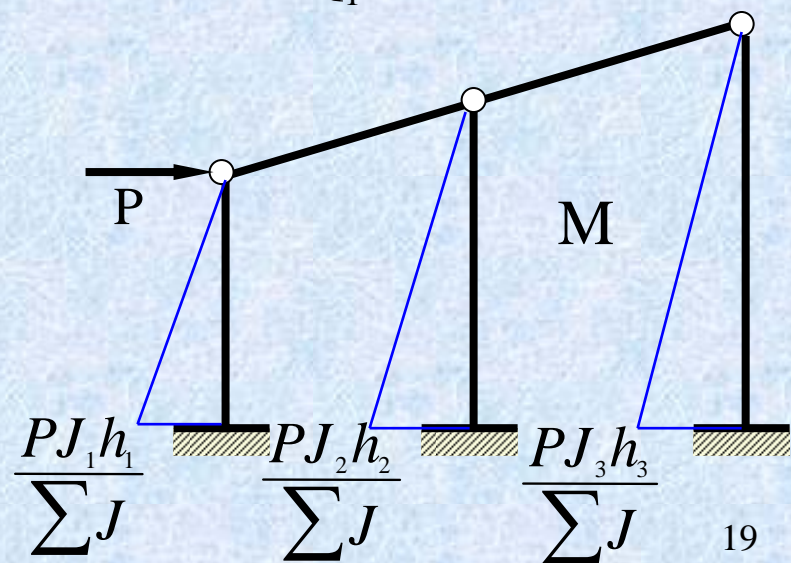
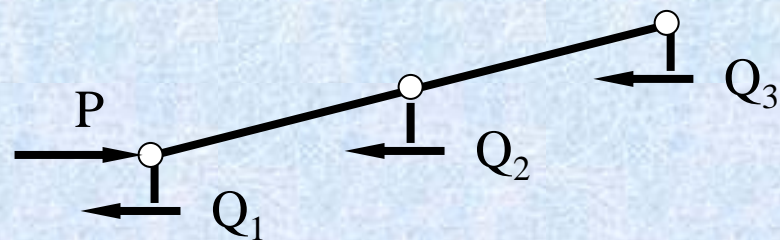
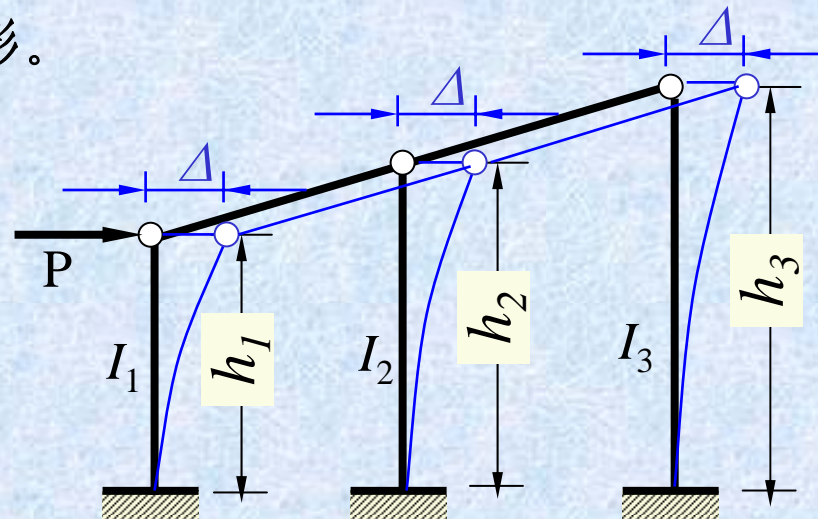
3) 位移法方程

$$\sum X=0 \quad Q_1+Q_2+Q_3=P$$

$$J_1\Delta + J_2\Delta + J_3\Delta = P \quad \Delta = \frac{P}{\sum J_i}$$

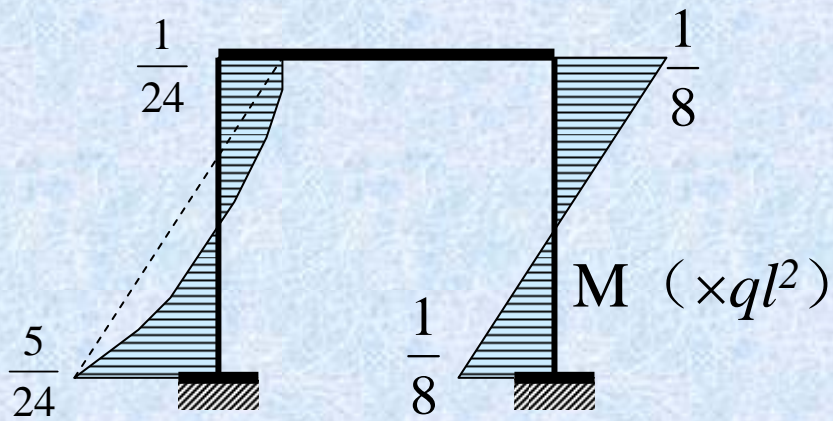
柱顶剪力： $Q_i = \frac{PJ_i}{\sum J}$

柱底弯矩： $M = Q_i h_i = \frac{PJ_i h_i}{\sum J}$



结点集中力作为各柱总剪力，按各柱的侧移刚度分配给各柱。再由反弯点开始即可作出弯矩图。

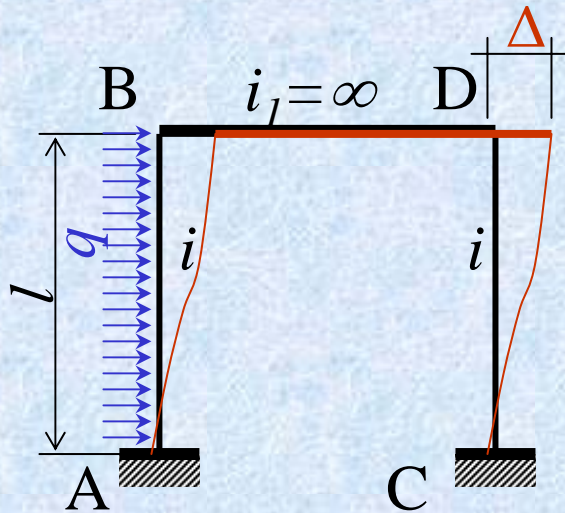
绘制弯矩图



$$M_{AB} = -\frac{6i}{l} \Delta + m_{AB} = -\frac{5}{24} ql^2$$

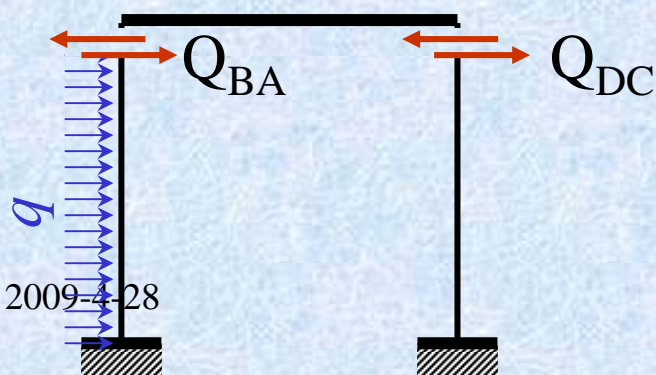
$$M_{BA} = -\frac{6i}{l} \Delta + m_{BA} = -\frac{1}{24} ql^2$$

.....



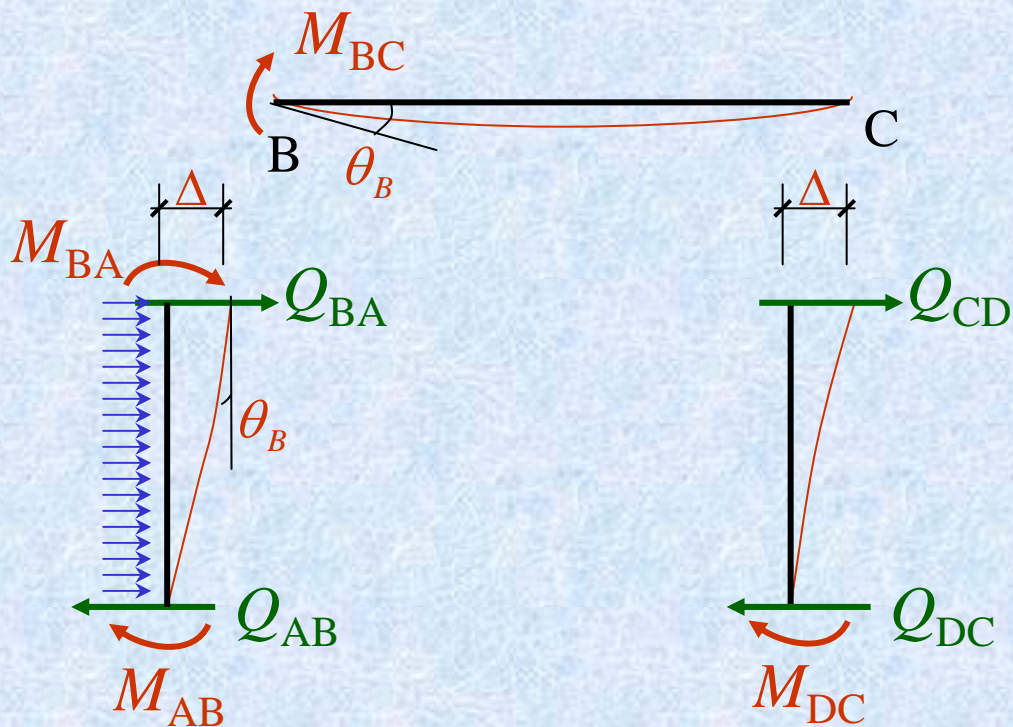
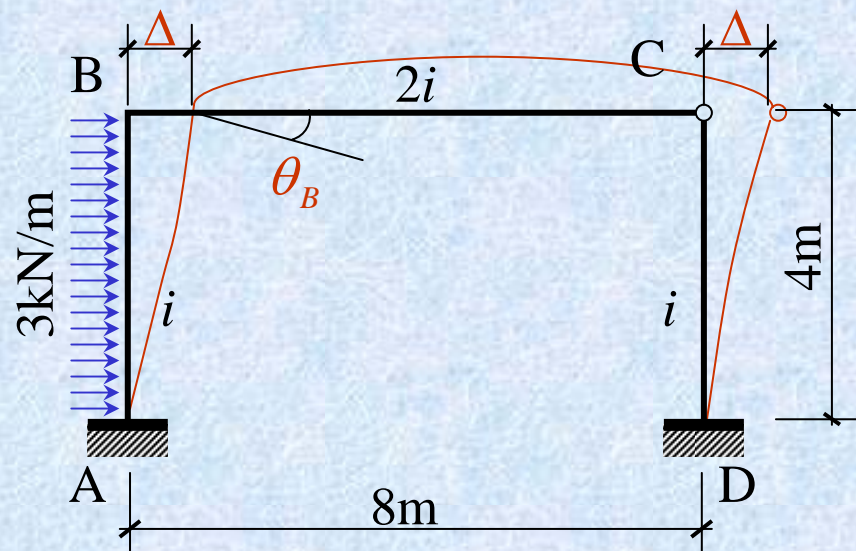
$$\sum x = 0 \quad Q_{BA} + Q_{DC} = 0$$

其中 $Q_{BA} = \frac{12i}{l^2} \Delta - \frac{ql}{2}$ $Q_{DC} = \frac{12i}{l^2} \Delta$



$$\frac{24i}{l^2} \Delta - \frac{ql}{2} = 0 \quad \Delta = \frac{ql^3}{48i}$$

例1. 用位移法分析图示刚架。



[解] (1) 基本未知量 θ_B 、 Δ

(2) 单元分析

$$M_{AB} = 2i\theta_B - \frac{6i}{4}\Delta - \frac{3 \times 4^2}{12}$$

$$M_{BC} = 3(2i)\theta_B$$

$$M_{BA} = 4i\theta_B - \frac{6i}{4}\Delta + \frac{3 \times 4^2}{12}$$

$$M_{DC} = -\frac{3i}{4}\Delta \quad Q_{CD} = \frac{3i}{4^2}\Delta$$

$$Q_{BA} = -\frac{6i}{4}\theta_B + \frac{12i}{4^2}\Delta - \frac{ql}{2} = 1.5i\theta_B + 0.75i\Delta - 6$$

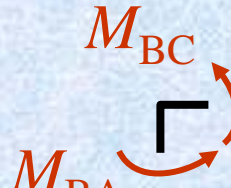
(3) 位移法方程

$$M_{AB} = 2i\theta_B - 1.5i\Delta - 4$$

$$M_{BA} = 4i\theta_B - 1.5i\Delta + 4$$

$$M_{BC} = 6i\theta_B$$

$$M_{DC} = -0.75i\Delta$$

$$\sum M_B = 0$$


$$M_{BA} + M_{BC} = 0 \dots \dots \dots (1a)$$

$$10i\theta_B - 15i\Delta + 4 = 0 \dots \dots \dots (1)$$

$$\sum x = 0$$

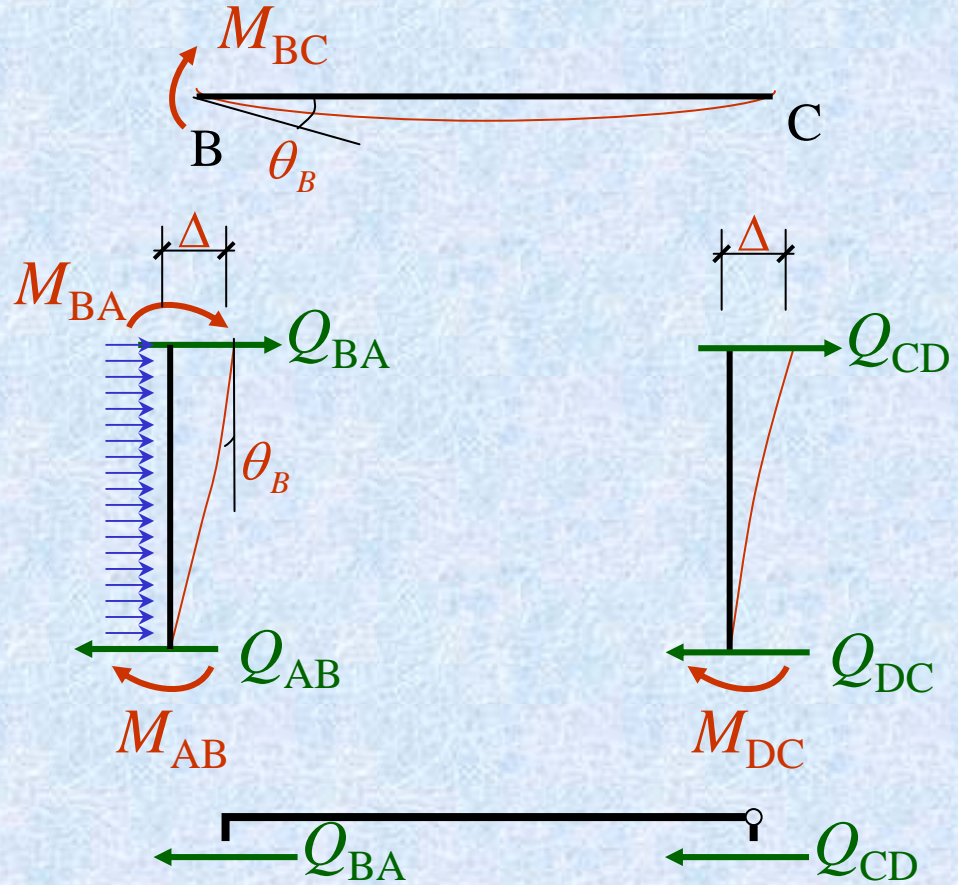
$$Q_{BA} + Q_{CD} = 0 \dots \dots \dots (2a)$$

$$6i\theta_B - 3.75i\Delta + 24 = 0 \dots \dots \dots (2)$$

(4) 解位移法方程

$$Q_{BA} = 1.5i\theta_B + 0.75i\Delta - 6$$

$$Q_{CD} = \frac{3i}{4} \Delta$$



(4) 解位移法方程

$$10i\theta_B - 1.5i\Delta + 4 = 0 \dots\dots\dots(1)$$

$$6i\theta_B - 3.75i\Delta + 24 = 0 \dots\dots\dots(2)$$

$$\theta_B = \frac{0.737}{i} \quad \Delta = \frac{7.58}{i}$$

(5) 弯矩图

$$M_{AB} = -13.896 \text{ kN}\cdot\text{m}$$

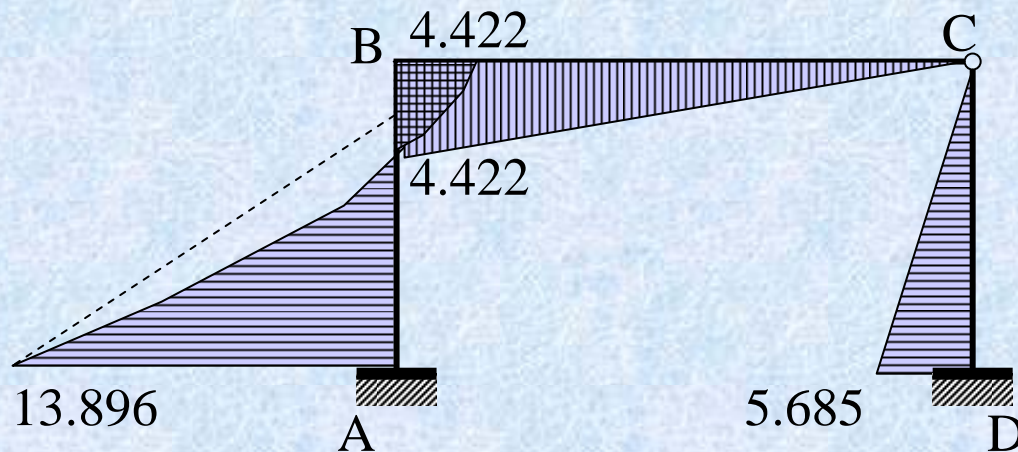
$$M_{BA} = -4.422 \text{ kN}\cdot\text{m}$$

$$M_{BC} = 4.422 \text{ kN}\cdot\text{m}$$

$$M_{DC} = -5.685 \text{ kN}\cdot\text{m}$$

$$Q_{BA} = -1.42 \text{ kN}$$

$$Q_{CD} = -1.42 \text{ kN}$$

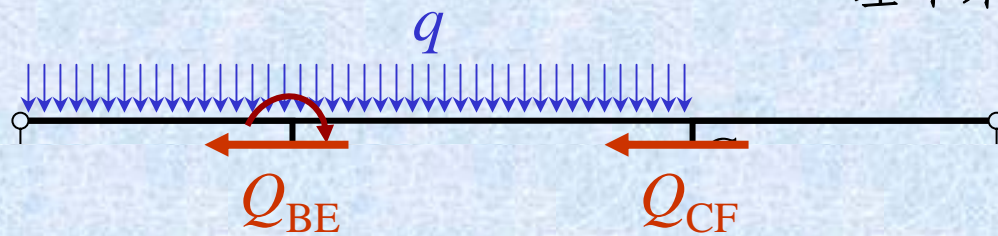


M图 (kN·m)



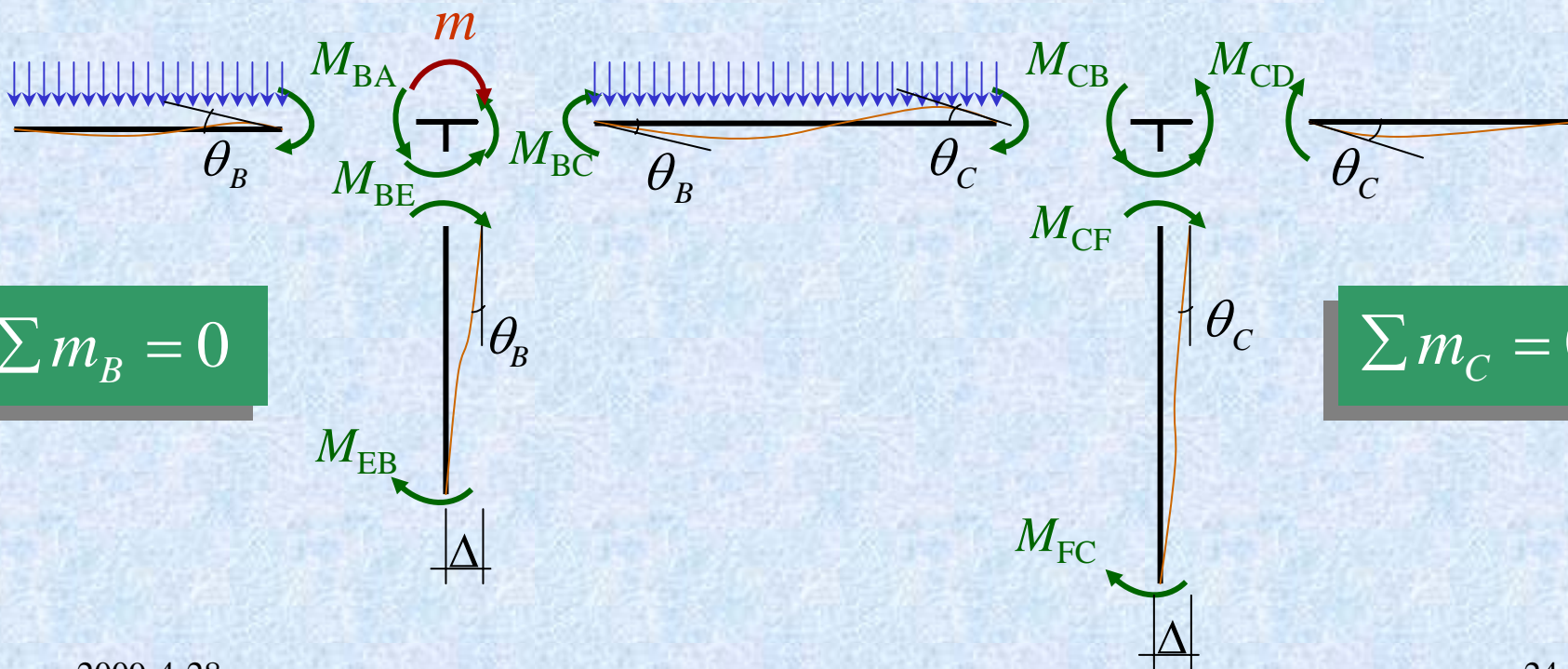
例2. 用位移法分析图示刚架。——思路

基本未知量为:



$\theta_B \quad \theta_C \quad \Delta$

$$\sum x = 0$$



$$\sum m_B = 0$$

$$\sum m_C = 0$$

基本未知量为: θ_C Δ

