# In situ rutile $\mathbf{U}-\mathbf{P b}$ dating by laser ablation-MC-ICPMS 

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#### Abstract

A method for in situ rutile $\mathrm{U}-\mathrm{Pb}$ dating was developed using a multiple-collector (MC) ICPMS coupled to an excimer laser-ablation system. Compared with single collector Quadruple ICPMS used by previous in situ rutile U-Pb dating studies, the Neptune Plus MC-ICPMS used in this study has higher sensitivity and is capable of simultaneous acquisition of all the isotope signals required for rutile $\mathrm{U}-\mathrm{Pb}$ dating. These advantages are important to achieve precise and reproducible in situ $\mathrm{U}-\mathrm{Pb}$ dating results for rutiles, which typically contain low abundances of U and radiogenic Pb . The analytical results in this study on three reference rutile standards (R10, JDX and DXK) and one nature rutile sample ( 07 RU 3 ) agree with literature/known values, thereby demonstrating that this technique can yield precise and accurate $\mathrm{U}-\mathrm{Pb}$ dating results for Paleozoic to Paleoproterozoic rutile, even with $\sim 1 \mathrm{ppm} U$.


Keywords: laser ablation, MC-ICPMS, rutile, $\mathrm{U}-\mathrm{Pb}$ dating, in situ

## InTRODUCTION

Laser ablation combined with inductively coupled plasma mass spectrometry (LA-ICP-MS) has been widely used in geochronological research in the last two decades. The LA-ICP-MS method has been widely applied to $\mathrm{U}-\mathrm{Pb}$ zircon dating, which can yield analytical precision comparable to that of the secondary ion microprobe (SIMS) technique (Horn et al., 2000; Simonetti et al., 2008; Xia et al., 2004). Rutile $\left(\mathrm{TiO}_{2}\right)$ is a common accessory mineral, which is common in many igneous, metamorphic and sedimentary rocks. It is stable over a wide range of $P-T$ conditions and is resistant to weathering, transportation and diagenesis (Morton and Hallsworth, 1994) and hosts measureable $U$ and radiogenic Pb . Previous studies have demonstrated that rutile can be used as a precise geochronometer and in particular has important applications for metamorphic rocks (Kylander-Clark et al., 2008; Li et al., 2011). Traditional isotope dilutionTIMS method has been applied to several $\mathrm{U}-\mathrm{Pb}$ rutile dating studies, although it often suffers from mineral inclusions and retrograde rims of titanite with high proportions of common lead (Xiao et al., 2006). Single collector LA-ICPMS has been employed for in situ $\mathrm{U}-\mathrm{Pb}$ rutile dating in pioneering works by Storey et al. (2007), Birch

[^0]et al. (2007), Zack et al. (2011) and Kooijman et al. (2010). This method is limited to rutile grains with sufficient U in order to get suitable Pb signal intensity (Zack et al., 2011). It is well known that multi collector ICPMS offers advantages in terms of higher sensitivity, flat top peak shape and simultaneous acquisition, features ideal for precise isotope ratio analyses. Some researchers have applied LA-MC-ICPMS to $\mathrm{U}-\mathrm{Pb}$ rutile dating such as Vry and Baker (2006), Warren et al. (2012) and Bracciali et al. (2013), but the amount of works using this method are limited, and Vry and Baker (2006) only obtained $\mathrm{Pb}-$ Pb ages and no $\mathrm{U}-\mathrm{Pb}$ ages. Therefore the potential of LA-MC-ICPMS to rutile $\mathrm{U}-\mathrm{Pb}$ dating has not been fully explored. We hereby report a new analytical protocol and the analytical results for 4 different natural rutile samples using LA-MC-ICPMS in this paper. Our results demonstrate that this technique can yield precise and accurate $\mathrm{U}-\mathrm{Pb}$ dating results for rutile even with $c a .1 \mathrm{ppm} \mathrm{U}$.

## Analytical Method

## Instrumentation

A Neptune Plus multi collector ICP-MS installed at the State Key Laboratory of Isotope Geochemistry, Guangzhou Institute of Geochemistry, Chinese Academy of Sciences (GIGCAS) was employed in this study. The MC-ICPMS is fitted with a collector block containing 9 variable position Faraday cups and 8 Ion Counters (compact discrete dynamic multiplier, CDD or SEM). This collector system has a relative mass range of more than
Laboratory and Sample Preparation
Laboratory name
Sample type/mineral
Sample preparation
Laser Ablation System
Make, model and type
Ablation cell and volume
Laser wavelength
Pulse width
Fluence
Repetition rate
Spot size
Sampling mode/pattern
Carrier gas
Ablation duration
ICP-MS Instrument
Make, model and type
Sample introduction
RF power
Make-up gas flow
Detection system
Masses measured
Data Processing
Gas blank
Calibration strategy
Reference Material info
Data processing package used
Uncertainty level and propagation
Other information

State Key Laboratory of Isotope Geochemistry, Guangzhou
Rutile
Conventional mineral separation, 1 inch resin mount

Resonetics LLC USA, RESOlution M-50, ArF excimer
Two-volume laser-ablation cell (Laurin Technic, Australia), effective volume $\sim 1-2 \mathrm{~cm}^{3}$
193 nm
$\sim 20 \mathrm{~ns}$
$4 \mathrm{~J} \cdot \mathrm{~cm}^{-2}$
5 Hz
44 um
Spot
$700 \mathrm{ml} / \mathrm{min} \mathrm{He}+2 \mathrm{ml} / \mathrm{min}_{2}$, Ar make-up gas
30 seconds

Thernmo Fisher Scientific, Neptune Plus, MC-ICP-MS
Ablation aerosol
1200 W
$400 \mathrm{ml} / \mathrm{min} \mathrm{Ar}$
Mixed Faraday-multiple ion counting array
202, 204, 206, 207, 208, 232238

30 seconds on-peak zero subtracted
R19 rutile standard used as primary reference material
$\mathrm{R} 19{ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U} 489.5 \pm 0.9 \mathrm{Ma},{ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb} 489.8 \pm 9.3 \mathrm{Ma}$ (Zack et al., 2011)
In-house created spreadsheet program
Ages are quoted at 2 sigma absolute, propagation is by quadratic addition.
Reproducibility and age uncertainty of reference material are propagated.
Sample line of 2.5 m from ablation cell to torch and a 30 seconds washout time after the laser stopped firing
$17 \%$, allowing simultaneous acquisition of ion signals ranging from mass ${ }^{202} \mathrm{Hg}$ to ${ }^{238} \mathrm{U}$, an important factor in obtaining highly precise and accurate $\mathrm{U}-\mathrm{Pb}$ age determinations. With a $100 \mu \mathrm{~L} / \mathrm{min}$ PFA standard concentric nebulizer, dual-pass spray chamber, standard sample cone and H -skimmer cone, this instrument commonly gives a sensitivity of $>1200 \mathrm{~V}$ for 1 ppm solution of ${ }^{238} \mathrm{U}$. The ICP-MS was equipped with an ArF excimer 193 nm RESOlution M-50 (Resonetics LLC, USA), which has been described in detail by Müller et al. (2009). This system can wash out $99 \%$ of the signal in less than 1.5 seconds due to its innovative sample cell design. Helium gas, which carries the laser-ablated sample aerosol from the sample cell, is mixed with argon carrier gas along with nitrogen as an additional di-atomic gas to enhance sensitivity, and finally flows into the MC-ICPMS torch. The operating conditions for this study are summarized in Table 1.

## Analytical protocols

Samples were prepared as grain mounts. The mounts were well polished to expose the fresh interior of the crys-
tals. Thorough cleaning were made by polishing the surface with alumina powder and then putting in an ultrasonic bath for 5 minutes with milli-Q water and finally drying with ethanol-soaked kimwipe paper.

Prior to analysis, gas flow rates of argon make-up gas, helium and nitrogen carrier gas were optimized to achieve maximum sensitivity with low oxide production $\left({ }^{254} \mathrm{UO} /\right.$ ${ }^{238} \mathrm{U}<1 \%$ ). Laser settings used for sample analyses include a beam diameter of $c a .44 \mu \mathrm{~m}, 5 \mathrm{~Hz}$ repetition rate, and energy intensity on target of about 4.0 J . The rutile was pre-ablated by five laser pulses before analysis in order to remove the surface common-lead contamination. Each analysis incorporated a background acquisition of approximately 30 seconds (gas blank, closing the laser shutter) followed by 30 seconds of data acquisition for the sample, which usually leave ablated pits with depth of $\sim 20 \mu \mathrm{~m} .{ }^{208} \mathrm{~Pb},{ }^{207} \mathrm{~Pb},{ }^{206} \mathrm{~Pb},{ }^{204} \mathrm{~Pb}\left(+{ }^{204} \mathrm{Hg}\right)$ and ${ }^{202} \mathrm{Hg}$ signals were measured on the ion counters, whereas ${ }^{238} \mathrm{U}$ and ${ }^{232} \mathrm{Th}$ were acquired on the Faraday cups. In order to check the linearity of the ion counters, the rutile R10 (see below) is ablated with variable laser fluences, spot size or repetition rate so as to achieve ${ }^{206} \mathrm{~Pb}$ signal from $<50000$



Fig. 1. Measured raw ratios of $\left.{ }^{206} \mathrm{~Pb}\right|^{238} U$ (a) and $\left.{ }^{207} \mathrm{~Pb}\right|^{206} \mathrm{~Pb}$ (b) for external calibration standard rutile R19. Data-point error bars are $1 \sigma$.
to $>1000000$ counts per second. Consistent common lead corrected ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ ratios with external precision of $<0.3 \%$ demonstrated a good linearity of the ion counters.

Corrections for instrumental drift, mass bias and ${ }^{206} \mathrm{~Pb} /$ ${ }^{238} \mathrm{U}$ fractionation were all conducted by a "standard-sample-standard" bracketing external standardization technique. One piece of standard rutile R19 with a size of $\sim 2 \times 1 \times 2 \mathrm{~mm}$ was used for this purpose. The crystal from which it is derived is a $c a .500 \mathrm{~mm}^{3}$ sized single crystal from Blumberg, Australia. Detailed trace elements, Hf isotope and $\mathrm{U}-\mathrm{Pb}$ age studies have been conducted for this standard (Luvizotto et al., 2009; Zack et al., 2011). A weighted mean ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ age of $489.5 \pm 0.9 \mathrm{Ma}$ obtained by the TIMS method (Zack et al., 2011) was adopted as the reference material in this study. It was analyzed three times every five analyses of unknown. A multi-collector ICPMS cannot measure an internal element standard if it requires a large mass jump such as needed for ${ }^{49} \mathrm{Ti}$, and so accurate U and Pb concentrations were impossible to obtain. However, in order to characterize the analyzed piece of rutile, approximate $U$ concentration data were obtained by direct comparing the signal intensities between the unknown and external standard NIST SRM 610 assuming they have the same signal yield for the same analytical conditions. NIST SRM 610 was analyzed twice every five analyses of unknown. The U concentration value of NIST SRM 610 used for external calibration was taken from Pearce et al. (1997).

Off-line data reduction (including selection and integration of background and analyte signals) was performed by a spreadsheet program created by the authors. The time-resolved signal of single isotopes and isotope ratios was carefully inspected to verify the presence of perturbations related to inclusions, fractures and mixing of different age domains. The mean ratios of ${ }^{232} \mathrm{Th} /{ }^{238} \mathrm{U}$,
${ }^{206} \mathrm{~Pb} /{ }^{208} \mathrm{~Pb},{ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ and ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ were calculated directly based on the background subtracted raw signals. No ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ fractionation is corrected for individual analyses besides the external standardization. The analytical uncertainties of the ratios were calculated based on standard deviation divided by square root of ( $n-1$ ), $n$ being the number of the time-resolved isotope ratios. Common-lead correction was performed by estimating the common-lead content based on the ${ }^{208} \mathrm{~Pb}$ signal intensity assuming all the ${ }^{208} \mathrm{~Pb}$ measured is non-radiogenic, as rutiles contain extremely low content of Th (Zack et al., 2011). A two-stage Pb evolution model of Stacey and Kramers (1975) was adopted. Time-dependent machine drift, mass bias and elemental fractionation were all corrected using a linear interpolation (with time) for every five analyses, according to the variations of the standard rutile R19.

In this study a dataset of 72 spot analyses were collected during about 6 hours for the external standard R19, which gave a reproducibility of $0.79 \%$ ( $95 \%$ confidence, MSWD $=0.44$ ) for ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ and $1.8 \%$ ( $95 \%$ confidence, MSWD $=0.17$ ) for ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ (Fig. 1). This uncertainty was propagated for each individual sample analysis following Horstwood et al. (2003). Therefore the ratio/age error quoted in the Table 2 comes from two sources: uncertainty of individual (single spot) analyses mainly due to counting statistics of the signals, and external standardization. The ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ ratio is derived from the normalized and error propagated ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ and ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ ratios assuming a ${ }^{238} \mathrm{U} /{ }^{235} \mathrm{U}$ natural abundance ratio of 137.88 , and the uncertainty is derived from the quadratic addition of the propagated uncertainties of both ratios. Concordia diagrams and weighted mean calculations were made using Isoplot V3.
Table 2. Rutile $U-P b$ analyzed by LA-MCICPMS

| Sample No. | U concentration | Corrected ratios |  |  |  |  |  |  |  | Errorcorrelations* | Ages |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Th/U | ${ }^{206} \mathrm{~Pb} /{ }^{208} \mathrm{~Pb}$ | ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ | $\begin{gathered} 1 \sigma \\ {[\%]} \end{gathered}$ |  | $\begin{gathered} 1 \sigma \\ {[\%]} \end{gathered}$ | ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ | $\begin{gathered} 1 \sigma \\ {[\%]} \end{gathered}$ |  | ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ | $2 \sigma_{\text {abs }}$ | ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ | $2 \sigma_{\text {abs }}$ | ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ | $2 \sigma_{\text {abs }}$ | $\begin{gathered} \text { Concordance** } \\ {[\%]} \end{gathered}$ |
| Rutile R10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| R10-1 | 45 | 0.0005 | 324 | 0.076 | 2.3 | 1.93 | 3.4 | 0.184 | 2.5 | 0.7 | 1099 | 45 | 1092 | 22 | 1088 | 25 | 100 |
| R10-2 | 45 | 0.0009 | 302 | 0.076 | 2.3 | 1.88 | 2.9 | 0.180 | 1.8 | 0.6 | 1083 | 46 | 1073 | 19 | 1068 | 18 | 100 |
| R10-3 | 45 | 0.0005 | 1158 | 0.076 | 3.3 | 1.96 | 3.8 | 0.187 | 1.9 | 0.5 | 1089 | 64 | 1100 | 25 | 1106 | 19 | 99 |
| R10-4 | 43 | 0.0004 | 408 | 0.076 | 2.4 | 1.97 | 3.0 | 0.189 | 1.8 | 0.6 | 1089 | 47 | 1106 | 20 | 1115 | 18 | 99 |
| R10-5 | 44 | 0.0005 | 63 | 0.075 | 2.8 | 1.90 | 4.3 | 0.183 | 3.3 | 0.8 | 1077 | 56 | 1080 | 28 | 1082 | 32 | 100 |
| R10-6 | 42 | 0.0001 | 72 | 0.076 | 2.7 | 1.90 | 3.9 | 0.183 | 2.7 | 0.7 | 1082 | 53 | 1083 | 25 | 1083 | 27 | 100 |
| R10-7 | 44 | 0.0001 | 73 | 0.075 | 3.2 | 1.94 | 4.6 | 0.187 | 3.3 | 0.7 | 1074 | 62 | 1093 | 30 | 1103 | 34 | 99 |
| R10-8 | 45 | 0.0002 | 60 | 0.075 | 2.8 | 1.91 | 3.4 | 0.185 | 2.0 | 0.6 | 1072 | 56 | 1086 | 23 | 1092 | 20 | 99 |
| R10-9 | 44 | 0.0000 | 95 | 0.076 | 2.9 | 1.96 | 3.8 | 0.188 | 2.5 | 0.7 | 1086 | 56 | 1101 | 25 | 1109 | 26 | 99 |
| R10-10 | 47 | 0.0006 | 436 | 0.076 | 2.4 | 1.91 | 4.0 | 0.183 | 3.2 | 0.8 | 1089 | 48 | 1086 | 26 | 1084 | 32 | 100 |
| R10-11 | 53 | 0.0003 | 567 | 0.076 | 2.4 | 1.92 | 2.8 | 0.183 | 1.5 | 0.5 | 1091 | 48 | 1088 | 19 | 1086 | 15 | 100 |
| R10-12 | 44 | 0.0006 | 154 | 0.076 | 2.6 | 1.92 | 3.8 | 0.183 | 2.8 | 0.7 | 1096 | 51 | 1087 | 25 | 1082 | 28 | 100 |
| R10-13 | 41 | 0.0001 | 84 | 0.075 | 3.2 | 1.92 | 4.1 | 0.186 | 2.7 | 0.6 | 1070 | 62 | 1089 | 27 | 1099 | 27 | 99 |
| R10-14 | 41 | 0.0009 | 108 | 0.076 | 2.3 | 1.90 | 4.2 | 0.181 | 3.6 | 0.8 | 1093 | 46 | 1080 | 28 | 1074 | 35 | 99 |
| R10-15 | 41 | 0.0005 | 89 | 0.076 | 2.5 | 1.91 | 3.6 | 0.183 | 2.6 | 0.7 | 1082 | 49 | 1084 | 24 | 1085 | 25 | 100 |
| R10-16 | 42 | 0.0001 | 235 | 0.076 | 2.3 | 1.92 | 4.0 | 0.184 | 3.3 | 0.8 | 1092 | 46 | 1090 | 27 | 1089 | 33 | 100 |
| R10-17 | 36 | 0.0003 | 1181 | 0.076 | 2.5 | 1.94 | 4.3 | 0.186 | 3.5 | 0.8 | 1093 | 49 | 1096 | 29 | 1098 | 36 | 100 |
| R10-18 | 40 | 0.0007 | 106 | 0.075 | 3.3 | 1.92 | 5.0 | 0.185 | 3.7 | 0.7 | 1078 | 65 | 1089 | 33 | 1095 | 38 | 99 |
| R10-19 | 45 | 0.0001 | 489 | 0.076 | 2.5 | 1.94 | 3.9 | 0.185 | 3.0 | 0.8 | 1100 | 49 | 1097 | 26 | 1095 | 30 | 100 |
| R10-20 | 41 | 0.0000 | 22 | 0.076 | 3.9 | 1.98 | 4.9 | 0.189 | 3.0 | 0.6 | 1091 | 77 | 1108 | 33 | 1116 | 31 | 99 |
| R10-21 | 35 | 0.0000 | 68 | 0.075 | 3.1 | 1.96 | 4.7 | 0.188 | 3.5 | 0.7 | 1081 | 61 | 1102 | 31 | 1112 | 36 | 99 |
| R10-22 | 42 | 0.0000 | 2833 | 0.076 | 3.1 | 1.89 | 4.9 | 0.181 | 3.7 | 0.8 | 1091 | 61 | 1079 | 32 | 1073 | 37 | 99 |
| R10-23 | 35 | 0.0001 | 42 | 0.075 | 2.9 | 1.96 | 4.5 | 0.189 | 3.5 | 0.8 | 1072 | 57 | 1101 | 30 | 1116 | 35 | 99 |
|  |  |  |  |  |  |  |  |  |  | Aver. | 1085.7 |  | 1090.9 |  | 1093.5 |  |  |
| Rutile DXK |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| DXK-1 | 8 | 0.0009 | 639 | 0.110 | 2.5 | 4.87 | 5.2 | 0.322 | 4.6 | 0.9 | 1793 | 45 | 1798 | 43 | 1802 | 72 | 100 |
| DXK-2 | 8 | 0.0112 | 380 | 0.109 | 2.7 | 4.77 | 5.8 | 0.316 | 5.1 | 0.9 | 1787 | 48 | 1779 | 47 | 1773 | 78 | 100 |
| DXK-3 | 8 | 0.0063 | 114 | 0.110 | 3.2 | 4.75 | 5.5 | 0.314 | 4.4 | 0.8 | 1793 | 58 | 1776 | 45 | 1761 | 68 | 99 |
| DXK-4 | 7 | 0.0001 | 266 | 0.109 | 3.7 | 4.77 | 7.2 | 0.316 | 6.1 | 0.9 | 1788 | 65 | 1779 | 58 | 1771 | 94 | 100 |
| DXK-5 | 8 | 0.0011 | 200 | 0.110 | 3.9 | 4.73 | 6.6 | 0.312 | 5.3 | 0.8 | 1797 | 69 | 1773 | 54 | 1752 | 81 | 99 |
| DXK-6 | 8 | 0.0014 | 187 | 0.110 | 3.4 | 4.69 | 5.7 | 0.309 | 4.6 | 0.8 | 1799 | 61 | 1765 | 47 | 1736 | 69 | 98 |
| DXK-7 | 9 | 0.0097 | 138 | 0.109 | 3.2 | 4.78 | 6.2 | 0.319 | 5.3 | 0.9 | 1777 | 57 | 1781 | 51 | 1784 | 82 | 100 |
| DXK-8 | 9 | 0.0073 | 200 | 0.109 | 3.4 | 4.80 | 6.2 | 0.318 | 5.3 | 0.8 | 1786 | 60 | 1784 | 51 | 1782 | 81 | 100 |
| DXK-9 | 4 | 0.0098 | 93 | 0.110 | 4.0 | 4.81 | 6.7 | 0.317 | 5.4 | 0.8 | 1803 | 71 | 1787 | 55 | 1773 | 83 | 99 |
| DXK-10 | 8 | 0.0036 | 447 | 0.110 | 3.0 | 4.84 | 5.4 | 0.320 | 4.6 | 0.8 | 1793 | 54 | 1792 | 45 | 1792 | 71 | 100 |
| DXK-11 | 8 | 0.0104 | 113 | 0.108 | 4.2 | 4.81 | 6.4 | 0.322 | 4.8 | 0.8 | 1774 | 75 | 1787 | 52 | 1798 | 75 | 99 |
| DXK-12 | 8 | 0.0155 | 113 | 0.108 | 3.9 | 4.73 | 6.5 | 0.319 | 5.2 | 0.8 | 1759 | 69 | 1773 | 53 | 1785 | 81 | 99 |
| DXK-13 | 10 | 0.0228 | 74 | 0.108 | 3.5 | 4.67 | 6.2 | 0.315 | 5.1 | 0.8 | 1762 | 62 | 1763 | 51 | 1763 | 79 | 100 |
| DXK-14 | 7 | 0.0051 | 364 | 0.109 | 2.6 | 4.85 | 5.3 | 0.323 | 4.6 | 0.9 | 1779 | 48 | 1793 | 44 | 1806 | 72 | 99 |
| DXK-15 | 11 | 0.0365 | 51 | 0.107 | 2.4 | 4.73 | 6.0 | 0.320 | 5.5 | 0.9 | 1751 | 43 | 1772 | 49 | 1789 | 85 | 99 |


| Sample No. | U concentration | Corrected ratios |  |  |  |  |  |  |  | Errorcorrelations* | Ages |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Th/U | ${ }^{206} \mathrm{~Pb} /{ }^{208} \mathrm{~Pb}$ | ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ | $\begin{gathered} \hline 1 \sigma \\ {[\%]} \end{gathered}$ | ${ }^{207} \mathrm{~Pb}{ }^{235} \mathrm{U}$ | $\begin{gathered} \hline 1 \sigma \\ {[\%]} \end{gathered}$ | ${ }^{206} \mathrm{~Pb}{ }^{238} \mathrm{U}$ | $\begin{gathered} 1 \sigma \\ {[\%]} \end{gathered}$ |  | ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ | $2 \sigma_{\text {abs }}$ | ${ }^{207} \mathrm{~Pb} /{ }^{\text {235 }} \mathrm{U}$ | $2 \sigma_{\text {abs }}$ | ${ }^{206} \mathrm{~Pb}{ }^{238} \mathrm{U}$ | $2 \sigma_{\text {abs }}$ | $\begin{gathered} \text { Concordance** } \\ {[\%]} \end{gathered}$ |
| DXK-16 | 8 | 0.0012 | 532 | 0.110 | 2.6 | 4.84 | 5.8 | 0.320 | 5.2 | 0.9 | 1796 | 47 | 1792 | 48 | 1788 | 81 | 100 |
| DXK-17 | 7 | 0.0072 | 224 | 0.110 | 3.2 | 4.83 | 5.7 | 0.320 | 4.7 | 0.8 | 1792 | 58 | 1790 | 47 | 1789 | 73 | 100 |
| DXK-18 | 8 | 0.0065 | 290 | 0.109 | 2.6 | 4.84 | 5.3 | 0.323 | 4.6 | 0.9 | 1775 | 46 | 1792 | 44 | 1807 | 73 | 99 |
| DXK-19 | 7 | 0.0053 | 875 | 0.110 | 2.7 | 4.89 | 4.8 | 0.324 | 4.0 | 0.8 | 1792 | 48 | 1801 | 40 | 1809 | 64 | 100 |
| DXK-20 | 8 | 0.0018 | 295 | 0.109 | 2.7 | 4.87 | 5.1 | 0.325 | 4.4 | 0.9 | 1777 | 48 | 1798 | 42 | 1816 | 69 | 99 |
| DXK-22 | 9 | 0.0215 | 89 | 0.107 | 3.0 | 4.60 | 5.3 | 0.312 | 4.4 | 0.8 | 1748 | 54 | 1749 | 44 | 1749 | 67 | 100 |
| DXK-23 | 8 | 0.0132 | 171 | 0.108 | 3.3 | 4.68 | 5.5 | 0.314 | 4.4 | 0.8 | 1771 | 59 | 1764 | 45 | 1758 | 67 | 100 |
| DXK-24 | 5 | 0.0107 | 110 | 0.109 | 3.4 | 4.80 | 5.8 | 0.319 | 4.7 | 0.8 | 1786 | 61 | 1785 | 47 | 1784 | 72 | 100 |
| DXK-25 | 7 | 0.0102 | 503 | 0.109 | 2.8 | 4.79 | 4.8 | 0.318 | 3.9 | 0.8 | 1790 | 50 | 1784 | 40 | 1779 | 61 | 100 |
| DXK-26 | 8 | 0.0002 | 402 | 0.109 | 3.0 | 4.68 | 5.9 | 0.312 | 5.1 | 0.9 | 1781 | 53 | 1763 | 48 | 1749 | 78 | 99 |
| DXK-27 | 7 | 0.0078 | 159 | 0.110 | 3.0 | 4.75 | 5.0 | 0.312 | 4.0 | 0.8 | 1806 | 53 | 1775 | 41 | 1749 | 62 | 99 |
| DXK-28 | 5 | 0.0055 | 282 | 0.110 | 3.6 | 4.74 | 5.7 | 0.313 | 4.4 | 0.8 | 1795 | 64 | 1775 | 47 | 1758 | 68 | 99 |
| DXK-29 | 8 | 0.0043 | 133 | 0.108 | 2.7 | 4.84 | 6.0 | 0.324 | 5.4 | 0.9 | 1773 | 48 | 1793 | 49 | 1809 | 84 | 99 |
| DXK-30 | 9 | 0.0151 | 191 | 0.108 | 2.7 | 4.79 | 5.6 | 0.321 | 5.0 | 0.9 | 1772 | 48 | 1784 | 46 | 1794 | 78 | 99 |
| DXK-31 | 6 | 0.0001 | 5092 | 0.110 | 2.8 | 4.83 | 5.1 | 0.318 | 4.2 | 0.8 | 1802 | 49 | 1790 | 42 | 1781 | 66 | 99 |
| DXK-32 | 6 | 0.0029 | 563 | 0.110 | 2.9 | 4.69 | 4.3 | 0.309 | 3.1 | 0.7 | 1801 | 52 | 1766 | 35 | 1737 | 47 | 98 |
| DXK-33 | 6 | 0.0088 | 7 | 0.109 | 2.7 | 4.86 | 5.3 | 0.322 | 4.5 | 0.9 | 1789 | 49 | 1795 | 44 | 1800 | 71 | 100 |
| DXK-34 | 9 | 0.0070 | 202 | 0.108 | 2.6 | 4.75 | 4.7 | 0.318 | 4.0 | 0.8 | 1774 | 47 | 1777 | 39 | 1779 | 61 | 100 |
| DXK-35 | 9 | 0.0047 | 12 | 0.109 | 3.4 | 4.76 | 5.3 | 0.318 | 4.0 | 0.8 | 1779 | 61 | 1779 | 43 | 1778 | 62 | 100 |
|  |  |  |  |  |  |  |  |  |  | Aver. | 1783.5 |  | 1781.0 |  | 1778.8 |  |  |
| Rutile JDX |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| JDX-1 | 14 | 0.0020 | 214 | 0.058 | 6.8 | 0.66 | 7.9 | 0.082 | 3.9 | 0.5 | 523 | 143 | 513 | 31 | 511 | 19 | 100 |
| JDX-2 | 14 | 0.0031 | 449 | 0.057 | 4.9 | 0.65 | 6.0 | 0.083 | 3.5 | 0.6 | 507 | 104 | 510 | 24 | 511 | 17 | 100 |
| JDX-3 | 10 | 0.0033 | 143 | 0.058 | 5.7 | 0.66 | 7.3 | 0.083 | 4.6 | 0.6 | 512 | 120 | 515 | 29 | 515 | 23 | 100 |
| JDX-4 | 12 | 0.0010 | 177 | 0.058 | 5.5 | 0.66 | 6.5 | 0.082 | 3.6 | 0.6 | 520 | 116 | 512 | 26 | 510 | 18 | 100 |
| JDX-5 | 13 | 0.0022 | 2345 | 0.058 | 3.7 | 0.66 | 4.7 | 0.083 | 3.0 | 0.6 | 519 | 79 | 516 | 19 | 515 | 15 | 100 |
| JDX-6 | 14 | 0.0012 | 407 | 0.058 | 5.0 | 0.66 | 5.7 | 0.084 | 2.8 | 0.5 | 516 | 106 | 517 | 23 | 517 | 14 | 100 |
| JDX-7 | 11 | 0.0012 | 245 | 0.057 | 6.0 | 0.65 | 7.2 | 0.082 | 3.9 | 0.5 | 505 | 127 | 510 | 28 | 511 | 19 | 100 |
| JDX-8 | 14 | 0.0029 | 85 | 0.058 | 5.8 | 0.66 | 6.9 | 0.082 | 3.7 | 0.5 | 535 | 122 | 514 | 27 | 509 | 18 | 99 |
| JDX-9 | 14 | 0.0000 | 955 | 0.058 | 3.7 | 0.65 | 4.9 | 0.082 | 3.2 | 0.7 | 530 | 80 | 510 | 20 | 506 | 16 | 99 |
| JDX-10 | 14 | 0.0003 | 332 | 0.058 | 4.5 | 0.65 | 5.4 | 0.082 | 3.1 | 0.6 | 535 | 95 | 511 | 22 | 505 | 15 | 99 |
| JDX-11 | 15 | 0.0014 | 179 | 0.057 | 5.6 | 0.66 | 6.6 | 0.083 | 3.5 | 0.5 | 508 | 118 | 512 | 26 | 513 | 17 | 100 |
| JDX-12 | 14 | 0.0025 | 148 | 0.058 | 5.5 | 0.66 | 6.7 | 0.082 | 3.9 | 0.6 | 525 | 115 | 512 | 27 | 509 | 19 | 99 |
| JDX-13 | 8 | 0.0023 | 300 | 0.058 | 5.2 | 0.67 | 7.4 | 0.083 | 5.3 | 0.7 | 528 | 110 | 518 | 30 | 515 | 26 | 100 |
| JDX-14 | 8 | 0.0016 | 285 | 0.057 | 5.0 | 0.64 | 6.2 | 0.081 | 3.7 | 0.6 | 505 | 106 | 502 | 24 | 501 | 18 | 100 |
| JDX-15 | 9 | 0.0075 | 68 | 0.057 | 6.2 | 0.63 | 8.7 | 0.080 | 6.1 | 0.7 | 501 | 132 | 499 | 34 | 499 | 29 | 100 |
| JDX-16 | 13 | 0.0020 | 237 | 0.058 | 4.0 | 0.65 | 5.6 | 0.082 | 4.0 | 0.7 | 513 | 85 | 509 | 22 | 508 | 19 | 100 |
| JDX-17 | 13 | 0.0015 | 1998 | 0.058 | 3.8 | 0.65 | 5.0 | 0.081 | 3.3 | 0.7 | 515 | 81 | 506 | 20 | 504 | 16 | 100 |
| JDX-18 | 13 | 0.0020 | 302 | 0.058 | 4.7 | 0.64 | 5.8 | 0.081 | 3.4 | 0.6 | 522 | 101 | 505 | 23 | 502 | 16 | 99 |
| JDX-19 | 12 | 0.0045 | 287 | 0.058 | 4.8 | 0.64 | 6.1 | 0.081 | 3.7 | 0.6 | 515 | 102 | 505 | 24 | 503 | 18 | 100 |
| JDX-20 | 12 | 0.0027 | 144 | 0.059 | 6.5 | 0.66 | 7.5 | 0.081 | 3.6 | 0.5 | 564 | 136 | 514 | 30 | 503 | 17 | 98 |

[^1]Table 2. (continued)

| Sample No. | U concentration | Corrected ratios |  |  |  |  |  |  |  | Error correlations* | Ages |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Th/U | ${ }^{206} \mathrm{~Pb} /{ }^{208} \mathrm{~Pb}$ | ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ | $\begin{gathered} 1 \sigma \\ {[\%]} \end{gathered}$ | ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ | $\begin{gathered} 1 \sigma \\ {[\%]} \end{gathered}$ | ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ | $\begin{gathered} 1 \sigma \\ {[\%]} \\ \hline \end{gathered}$ |  | ${ }^{207} \mathrm{~Pb} /{ }^{206} \mathrm{~Pb}$ | $2 \sigma_{\text {abs }}$ | ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ | $2 \sigma_{\text {abs }}$ | ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ | $2 \sigma_{\text {abs }}$ | Concordance** [\%] |
| JDX-21 | 12 | 0.0343 | 4 | 0.058 | 4.2 | 0.65 | 6.5 | 0.082 | 4.9 | 0.8 | 540 | 89 | 511 | 26 | 505 | 24 | 99 |
| JDX-22 | 11 | 0.0026 | 224 | 0.057 | 6.4 | 0.65 | 7.4 | 0.082 | 3.7 | 0.5 | 503 | 134 | 508 | 29 | 510 | 18 | 100 |
| JDX-23 | 12 | 0.0008 | 506 | 0.058 | 4.2 | 0.65 | 5.7 | 0.082 | 3.8 | 0.7 | 517 | 90 | 509 | 22 | 507 | 18 | 100 |
| JDX-24 | 12 | 0.0022 | 186 | 0.058 | 7.2 | 0.64 | 7.9 | 0.081 | 3.4 | 0.4 | 514 | 150 | 503 | 31 | 500 | 16 | 99 |
| JDX-25 | 12 | 0.0382 | 3 | 0.058 | 4.3 | 0.65 | 5.5 | 0.081 | 3.5 | 0.6 | 544 | 91 | 508 | 22 | 500 | 17 | 98 |
| JDX-26 | 12 | 0.0001 | 350 | 0.058 | 5.2 | 0.66 | 6.1 | 0.083 | 3.2 | 0.5 | 517 | 111 | 515 | 24 | 514 | 16 | 100 |
| JDX-27 | 13 | 0.0015 | 208 | 0.058 | 6.3 | 0.66 | 7.5 | 0.082 | 4.2 | 0.6 | 533 | 131 | 514 | 30 | 510 | 20 | 99 |
| JDX-28 | 13 | 0.0024 | 2832 | 0.058 | 3.6 | 0.67 | 5.2 | 0.084 | 3.8 | 0.7 | 515 | 76 | 521 | 21 | 522 | 19 | 100 |
| JDX-29 | 12 | 0.0016 | 3653 | 0.058 | 4.1 | 0.66 | 5.7 | 0.083 | 4.0 | 0.7 | 515 | 87 | 513 | 23 | 512 | 20 | 100 |
| JDX-30 | 12 | 0.0011 | 210 | 0.058 | 6.3 | 0.66 | 7.4 | 0.083 | 3.8 | 0.5 | 532 | 133 | 516 | 29 | 513 | 19 | 99 |
| JDX-31 | 12 | 0.0035 | 580 | 0.058 | 5.2 | 0.66 | 6.5 | 0.083 | 3.8 | 0.6 | 513 | 111 | 512 | 26 | 512 | 19 | 100 |
| JDX-32 | 9 | 0.0000 | 3092 | 0.058 | 4.4 | 0.67 | 6.6 | 0.083 | 4.9 | 0.7 | 540 | 94 | 519 | 26 | 514 | 24 | 99 |
| JDX-33 | 9 | 0.0000 | -2314 | 0.058 | 4.8 | 0.67 | 7.1 | 0.084 | 5.3 | 0.7 | 521 | 101 | 522 | 29 | 522 | 27 | 100 |
| JDX-34 | 8 | 0.0000 | -2330 | 0.057 | 4.4 | 0.67 | 6.3 | 0.084 | 4.5 | 0.7 | 503 | 93 | 519 | 25 | 522 | 22 | 99 |
|  |  |  |  |  |  |  |  |  |  | Aver. | 520.7 |  | 511.5 |  | 509.7 |  |  |
| Rutile 07RU3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07RU3-1 | 1.1 | 0.0000 | 17 | 0.053 | 17.9 | 0.38 | 18.4 | 0.052 | 4.2 | 0.2 | 309 | 364 | 325 | 50 | 327 | 13 | 99 |
| 07RU3-2 | 1.1 | 0.0000 | 6 | 0.053 | 20.6 | 0.38 | 22.1 | 0.052 | 8.0 | 0.4 | 343 | 409 | 327 | 60 | 324 | 25 | 99 |
| 07RU3-3 | 1.1 | 0.0000 | 18 | 0.053 | 15.8 | 0.37 | 16.3 | 0.051 | 4.0 | 0.2 | 313 | 324 | 322 | 44 | 323 | 13 | 100 |
| 07RU3-4 | 1.2 | 0.0001 | 25 | 0.055 | 17.8 | 0.40 | 18.4 | 0.053 | 4.6 | 0.3 | 428 | 355 | 343 | 52 | 330 | 15 | 96 |
| 07RU3-5 | 1.2 | 0.0000 | 3 | 0.052 | 17.1 | 0.37 | 18.7 | 0.051 | 7.4 | 0.4 | 266 | 352 | 317 | 50 | 324 | 23 | 98 |
| 07RU3-6 | 1.2 | 0.0001 | 14 | 0.051 | 17.3 | 0.37 | 17.7 | 0.052 | 3.8 | 0.2 | 224 | 357 | 316 | 47 | 329 | 12 | 96 |
| 07RU3-7 | 1.1 | 0.0000 | 24 | 0.051 | 21.3 | 0.35 | 21.7 | 0.051 | 4.2 | 0.2 | 219 | 431 | 307 | 56 | 319 | 13 | 96 |
| 07RU3-8 | 1.1 | 0.0000 | 12 | 0.053 | 17.5 | 0.37 | 18.0 | 0.051 | 4.4 | 0.2 | 309 | 356 | 317 | 48 | 318 | 14 | 100 |
| 07RU3-9 | 1.0 | 0.0011 | 1 | 0.052 | 14.3 | 0.36 | 15.2 | 0.051 | 5.0 | 0.3 | 290 | 298 | 315 | 40 | 318 | 15 | 99 |
| 07RU3-10 | 1.0 | 0.0011 | 1 | 0.052 | 14.3 | 0.37 | 15.2 | 0.051 | 5.0 | 0.3 | 299 | 298 | 319 | 41 | 321 | 16 | 99 |
| 07RU3-11 | 1.0 | 0.0034 | 2 | 0.049 | 15.5 | 0.35 | 16.0 | 0.052 | 3.7 | 0.2 | 147 | 329 | 307 | 41 | 329 | 12 | 93 |
| 07RU3-12 | 1.1 | 0.0002 | 72 | 0.050 | 16.9 | 0.37 | 17.4 | 0.053 | 4.0 | 0.2 | 193 | 351 | 317 | 46 | 334 | 13 | 95 |
| 07RU3-13 | 0.9 | 0.0000 | 18 | 0.052 | 16.8 | 0.37 | 17.3 | 0.052 | 4.1 | 0.2 | 268 | 346 | 322 | 47 | 329 | 13 | 98 |
| 07RU3-14 | 1.0 | 0.0000 | 11 | 0.048 | 16.9 | 0.35 | 17.4 | 0.052 | 4.0 | 0.2 | 122 | 356 | 304 | 45 | 328 | 13 | 93 |
| 07RU3-15 | 0.8 | 0.0044 | 1 | 0.052 | 12.5 | 0.36 | 12.9 | 0.050 | 3.3 | 0.3 | 277 | 263 | 313 | 34 | 317 | 10 | 98 |
| 07RU3-16 | 1.1 | 0.0004 | 10 | 0.056 | 17.5 | 0.40 | 18.0 | 0.052 | 4.1 | 0.2 | 437 | 348 | 339 | 50 | 325 | 13 | 96 |
| 07RU3-17 | 1.1 | 0.0001 | 7 | 0.052 | 18.2 | 0.36 | 19.0 | 0.051 | 5.3 | 0.3 | 284 | 370 | 315 | 50 | 319 | 16 | 99 |
| 07RU3-18 | 1.1 | 0.0002 | 5 | 0.050 | 12.9 | 0.37 | 13.6 | 0.053 | 4.3 | 0.3 | 213 | 274 | 317 | 36 | 331 | 14 | 96 |
| 07RU3-19 | 1.0 | 0.0006 | 2 | 0.052 | 18.1 | 0.38 | 18.6 | 0.053 | 4.2 | 0.2 | 300 | 368 | 327 | 51 | 331 | 14 | 99 |
| 07RU3-20 | 1.0 | 0.0025 | 1 | 0.055 | 13.4 | 0.39 | 14.0 | 0.051 | 4.1 | 0.3 | 418 | 274 | 333 | 39 | 321 | 13 | 96 |
| 07RU3-21 | 1.0 | 0.0000 | 25 | 0.049 | 18.9 | 0.35 | 19.4 | 0.052 | 4.1 | 0.2 | 127 | 394 | 304 | 50 | 328 | 13 | 93 |
| 07RU3-22 | 1.2 | 0.0000 | 14 | 0.047 | 21.3 | 0.34 | 21.8 | 0.052 | 4.9 | 0.2 | 69 | 441 | 297 | 55 | 326 | 16 | 91 |
| 07RU3-23 | 1.1 | 0.0000 | 14 | 0.050 | 17.9 | 0.36 | 18.4 | 0.052 | 4.2 | 0.2 | 206 | 370 | 310 | 48 | 324 | 13 | 96 |
| 07RU3-24 | 1.1 | 0.0000 | 40 | 0.054 | 18.1 | 0.39 | 18.5 | 0.053 | 3.4 | 0.2 | 366 | 364 | 335 | 51 | 330 | 11 | 99 |
|  |  |  |  |  |  |  |  |  |  | Aver. | 267.8 |  | 318.7 |  | 325.2 |  |  |

[^2]$*^{* *}$ Concordance is calculated as $100-100 *$ abs $\left({ }^{207} \mathrm{~Pb}^{235} \mathrm{U} \text { age }-\left.{ }^{206} \mathrm{~Pb}\right|^{238} \mathrm{U} \text { age) }\right)^{206} \mathrm{~Pb}{ }^{238} \mathrm{U}$ age .


Fig. 2. U-Pb concordia diagrams showing the analytical results for standard rutiles R10 (a), DKX (b), JDX (c) and the unknown sample $07 R U 3(d)$. Data-point error ellipses are $1 \sigma . M S W D$ is the mean square of weighted deviations.

## Results and Discussion

Secondary rutile standards used in this study are one international rutile standard (R10) (Luvizotto et al., 2009), two in-house rutile standards (JDX and DXK) (Li et al., 2011) and one unknown nature rutile sample 07RU3. The analytical results obtained in this study are listed in the Table 2.

## Rutile standard R10

This rutile has been widely used in LA-ICPMS and SIMS labs for $\mathrm{U}-\mathrm{Pb}$ isotope analyses (Kooijman et al., 2010; Li et al., 2011; Zack et al., 2011). A piece of R10 rutile fragment separated from a large single crystal was used in this study. TIMS analyses for this rutile yield relatively high U concentration ( $c a .50 \mathrm{ppm}$ ) and rather constant $\mathrm{U}-\mathrm{Pb}$ age ranging from 1086.3 to $1096.6 \mathrm{Ma}\left({ }^{206} \mathrm{~Pb} /\right.$ ${ }^{238} \mathrm{U}$ age $)$ and from 1085.1 to $1096.2 \mathrm{Ma}\left({ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}\right.$ age $)$ (Luvizotto et al., 2009). The $23 \mathrm{U}-\mathrm{Pb}$ spot analyses for
this rutile obtained in this study are shown on the Concordia diagram (Fig. 2a), yielding a Concordia age of $1091.5 \pm 9.6 \mathrm{Ma}(2 \sigma$, decay constant errors included, MSWD $=0.21$, Fig. 2a), which is vary consistent with the TIMS results. The weighted mean ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ age is $1093 \pm 10 \mathrm{Ma}(95 \%$ confidence, MSWD $=0.33$, Fig. 3a) and the weighted mean ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ age is $1090 \pm 10 \mathrm{Ma}$ ( $95 \%$ confidence, MSWD $=0.14$, Fig. $3 b$ ). Both ages are within the range of the reported TIMS ages.

## Rutile standard DXK

This studied rutile comes from a rutile deposit located in Henshan Mountain of the Trans-North China Orogen, which has been described by Shi et al. (2012). It is one of the largest rutile deposits in China, with a resource of 6 million metric tons of titanium. Rutiles are hosted mainly by anthophyllite gneisses and mostly occur as euhedral tetragonal crystals or fragments with lengths ranging from 0.02 to 0.50 mm . They are mostly translucent and dark


Fig. 3. Corrected ratios of ${ }^{206} \mathrm{~Pb}{ }^{238} \mathrm{U}$ and ${ }^{207} \mathrm{~Pb}{ }^{235} U$ for standard rutiles $R 10(a, b), D K X(c, d), J D X(e, f)$ and unknown sample $07 R U 3$ ( $g$, h). Data-point error bars are $1 \sigma$.
red to dark brown. Thirty rutile grains or fragments have been analyzed previously by Shi et al. using the SIMS method (sample RZ-1) (Shi et al., 2012). Their results indicate different rutile grains from this sample have rela-
tively consistent and high U concentrations ( $\sim 20 \mathrm{ppm}$ ) and almost identical $\mathrm{U}-\mathrm{Pb}$ isotopic compositions, thus it is suitable to be used as an in house standard for quality control of in situ $\mathrm{U}-\mathrm{Pb}$ rutile dating studies. The weighted
mean SIMS ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ age is $1779 \pm 13 \mathrm{Ma}(95 \%$ confidence, MSWD $=0.73$ ) and the weighted mean of SIMS ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ age is $1775 \pm 23 \mathrm{Ma}$ ( $95 \%$ confidence, MSWD $=0.75$ ) (Shi et al., 2012). Thirty five rutile grains analyzed in this study comes from the same sample (RZ-1) analyzed by Shi et al. (2012). Our analytical results for this sample gave a Concordia age of $1781 \pm 15 \mathrm{Ma}(2 \sigma$, decay constant errors included, MSWD $=0.17$, Fig. 2 b ) with a weighted mean ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ age of $1777 \pm 24 \mathrm{Ma}(95 \%$ confidence, MSWD $=0.102$, Fig. 3c) and a weighted mean ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ age of $1781 \pm 15 \mathrm{Ma}$ ( $95 \%$ confidence, MSWD $=0.074)$. These results are very similar to the SIMS results.

## Rutile standard JDX

Rutile JDX is a large gem-grade euhedral crystal, which is 5 cm in length and 2.5 cm in thickness. This rutile has been used as an in-house standard for SIMS analyses by the Institute of Geology and Geophysics, Chinese Academy of Sciences, Beijing (Li et al., 2011). Previous SIMS analyses on this rutile show that it contains $5-10 \mathrm{ppm}$ of U and yields a weighted mean ${ }^{207} \mathrm{~Pb} /$ ${ }^{235} \mathrm{U}$ age of $513 \pm 9 \mathrm{Ma}$ and a weighted mean ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ age of $509 \pm 8 \mathrm{Ma}$ (Li et al., 2011). In this study thirty four spots were analyzed on eight small fragments ( $\sim 300$ $\times 300 \times 200 \mu \mathrm{~m})$ in one mount. The $\mathrm{U}-\mathrm{Pb}$ data cluster together on the Concordia diagram with a Concordia age $509.7 \pm 6.2 \mathrm{Ma}$ ( $2 \sigma$, decay constant errors included, MSWD $=0.37$, Fig. 2c) and yield a weighted mean ${ }^{206} \mathrm{~Pb} /$ ${ }^{238} \mathrm{U}$ age of $509.3 \pm 6.1 \mathrm{Ma}(95 \%$ confidence, $\mathrm{MSWD}=$ 0.107 , Fig. 3e) and a weighted mean ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ age of $511.7 \pm 8.3 \mathrm{Ma}(95 \%$ confidence, MSWD $=0.041$, Fig. $3 f$ ), which are within the error of the SIMS age.

## Rutile sample 07RU3

The sample 07RU3 was collected from the eclogite block along the Akyazhi River, southwestern Chinese Tianshan. It is a rutile-bearing vein and the rutiles are centimeter-sized oriented acicular. Previous SIMS results for a single large crystal ( $\sim 5 \mathrm{~cm}$ in diameter) from this sample indicated it has relatively uniform $U$ content of $1.5 \pm 0.3 \mathrm{ppm}(1 \mathrm{SD})\left(\right.$ Li et al., 2011). Applying a ${ }^{207} \mathrm{~Pb}$ based common lead correction method yields a weighted mean ${ }^{206} \mathrm{~Pb} /{ }^{238} \mathrm{U}$ age of $320 \pm 10 \mathrm{Ma}(95 \%$ confidence, MSWD $=2.0$, SIMS method) (Li et al., 2011). Twenty four rutile grains from the same mount were analyzed in this study. The $\mathrm{U}-\mathrm{Pb}$ data are displayed on the Concordia diagram (Fig. 2d), which yields a Concordia age of 325.2 $\pm 5.6 \mathrm{Ma}(2 \sigma$, decay constant errors included, MSWD $=$ 0.56 , Fig. 2d). These data give a weighted mean ${ }^{206} \mathrm{~Pb} /$ ${ }^{238} \mathrm{U}$ age of $325.4 \pm 5.4$ ( $95 \%$ confidence, $\mathrm{MSWD}=0.14$, Fig. 3 g ) and ${ }^{207} \mathrm{~Pb} /{ }^{235} \mathrm{U}$ age of $318 \pm 18(95 \%$ confidence, MSWD $=0.055$, Fig. 3h), consistent with the previous SIMS results.

## Conclusions

This paper reports a new rutile $\mathrm{U}-\mathrm{Pb}$ dating protocol using a MC-ICPMS coupled with an excimer 193 nm laser ablation system and its successful application to three reference rutile standards (R10, JDX and DXK) and one rutile sample (07RU3). The analytical results obtained by this protocol agree well with literature values or previous results, thereby demonstrating that this technique can yield precise and accurate $\mathrm{U}-\mathrm{Pb}$ dating results for Paleozoic to Paleoproterozoic rutile even with $\sim 1 \mathrm{ppm}$ U.

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[^1]:    

[^2]:    *Error correlation is calculated as ${ }^{207} \mathrm{~Pb}^{235} U_{\text {error }}{ }^{2}+\left.{ }^{206} \mathrm{~Pb}\right|^{238} U^{2}-\left.{ }^{207} \mathrm{~Pb}\right|^{206} \mathrm{~Pb}$ error $\left.{ }^{2}\right) /\left(\left.\left.2 *^{207} \mathrm{~Pb}\right|^{235} U^{* 206} \mathrm{~Pb}\right|^{238} U\right)$,

