Chinese Journal of Catalysis

Vol. 33 No. 2

文章编号: 0253-9837(2012)02-0281-09

国际版 DOI: 10.1016/S1872-2067(11)60335-5

柠檬酸络合法制备的 Co/CeO2 催化剂上中温乙醇水蒸气重整性能

庞潇健,陈亚中*,代瑞旗,崔 鹏

合肥工业大学化工学院,安徽合肥230009

摘要:采用柠檬酸络合法制备了 Co/CeO₂ 及其钙掺杂系列催化剂,并对催化剂进行了低温 N₂ 物理吸附、X 射线衍射、H₂程序 升温还原、傅里叶变换红外光谱、高分辨透射电镜表征以及乙醇水蒸气重整催化性能测试.结果表明,所制 Co/CeO₂ 催化剂具 有良好的乙醇水蒸气重整催化性能,500 °C 时乙醇能全部转化为 C₁,氢气产率高达 85% 以上.Ca 掺杂减小了载体 CeO₂ 纳米 颗粒尺寸,但对还原后 Co⁰ 尺寸的影响较小.当 Ca 掺杂量大于 5.0% 时,催化剂氧化还原性能和乙醇水蒸气重整催化性能下 降.较高的还原温度有利于体相 Ce⁴⁺ 还原为 Ce³⁺,并且提高了催化活性,认为金属-氧化物边界的增加提高了催化活性.初步 稳定性考察结果表明,5% 钙掺杂后的催化剂具有更好的抗积炭性能.

关键词: 钴; 氧化铈; 氧化钙掺杂; 柠檬酸络合; 乙醇水蒸气重整; 中温

中图分类号: O643 文献标识码: A

收稿日期: 2011-09-15. 接受日期: 2011-10-26.

*通讯联系人. 电话: (0551)2901450; 电子信箱: chenyazhong@hfut.edu.cn

基金来源: 国家自然科学基金(20876030); 安徽省自然科学基金(110406Q31).

本文的英文电子版(国际版)由Elsevier出版社在ScienceDirect上出版(http://www.sciencedirect.com/science/journal/18722067).

Co/CeO₂ Catalysts Prepared Using Citric Acid Complexing for Ethanol Steam Reforming

PANG Xiaojian, CHEN Yazhong*, DAI Ruiqi, CUI Peng

School of Chemical Engineering, Hefei University of Technology, Hefei 230009, Anhui, China

Abstract: Co/CeO₂ catalysts with and without calcium doping were prepared by the citric acid complexing method, and characterized by N_2 adsorption, X-ray diffraction, temperature-programmed reduction, Fourier transform infrared spectroscopy, and high resolution transmission electron microscope. Their catalytic performance measurement for ethanol steam reforming (ESR) at 400–650 °C and atmospheric pressure with a steam-to-carbon ratio of 3.0 and gas hourly space velocity of 50000 ml/(g·h) was measured. The citric acid complexing method enhanced metal-support interaction. The Co/CeO₂ catalysts gave almost 100% ethanol conversion and good hydrogen yield at 500 °C. Calcium doping in the catalyst reduced the particle size of CeO₂, but had little effect on the metallic cobalt size after reduction. Calcium doping higher than 5% deteriorated the redox properties and ESR catalytic performance, which was attributed to the fouling of CeO₂ by CaO. Catalysts activated at 650 °C showed a better performance, which was due to a higher reduction degree of ceria and increase of the metal-oxide interface. Stability investigation of the catalysts suggested that 5% calcium doping enhanced carbon deposition resistance.

Key words: cobalt; ceria; calcium doping; citric acid complexing; ethanol steam reforming; intermediate temperature

Received 15 September 2011. Accepted 26 October 2011.

*Corresponding author. Tel: +86-551-2901450; E-mail: chenyazhong@hfut.edu.cn

This work was supported by the National Natural Science Foundation of China (20876030) and Natural Science Foundation of Anhui Province (110406Q31).

English edition available online at Elsevier ScienceDirect (http://www.sciencedirect.com/science/journal/18722067).

Hydrogen production from various hydrocarbon and alcohol fuels has been a focus of investigation recently [1]. Bio-ethanol from the fermentation of organic matter is environmentally sustainable and benign [2]. Ethanol steam

reforming (ESR) occurs by a complex mechanism. The following reactions take place, which include the desired ESR (Eq. 1), ethanol decomposition (Eq. 2), water gas shift (Eq. 3), ethanol dehydrogenation (Eq. 4), ethanol dehydration (Eq. 5), methanation (Eq. 6), and carbon deposition (Eqs. 7, 8).

 $C_2H_5OH + 3H_2O \rightarrow 2CO_2 + 6H_2$ $\Delta H^{0}_{298} = 173.1 \text{ kJ/mol}(1)$ $\Delta H^{0}_{298} = 49 \text{ kJ/mol} (2)$ $C_2H_5OH \rightarrow CO + CH_4 + H_2$ $\Delta H^{0}_{298} = -41 \text{ kJ/mol}(3)$ $CO + H_2O \leftrightarrow CO_2 + H_2$ $\Delta H^{0}_{298} = 68 \text{ kJ/mol} (4)$ $C_2H_5OH \rightarrow H_2 + CH_3CHO$ $C_2H_5OH \rightarrow C_2H_4 + H_2O$ $\Delta H^{0}_{298} = 45 \text{ kJ/mol}(5)$ $\Delta H^{0}_{298} = -205 \text{ kJ/mol}(6)$ $CO + 3H_2 \leftrightarrow CH_4 + H_2O$ $\Delta H^{0}_{298} = -171.5 \text{ kJ/mol}(7)$ $2CO \rightarrow C + CO_2$ $C_2H_4 \rightarrow polymers \rightarrow coke$ (8)

Although the thermodynamics of ESR suggest a simple reaction with few byproducts, under kinetically controlled conditions, the reaction network is very complex and the product distribution depends on the catalyst used [3,4]. Supported catalysts containing Ni, Cu, Co, and noble metals such as Rh, Ru, Ir, and Pt have been used for ESR [5-12]. Supported noble metal catalysts show good activity for ESR, but their high costs limit their application. A much cheaper alternative is cobalt-based catalysts, which also show good performance for ESR due to their high activity for C-C bond cleavage and good selectivity to hydrogen at temperatures as low as 350-400 °C [14,15]. For example, over a Co/ZnO catalyst at 350 °C, an ethanol conversion of 100% was achieved at gas hourly space velocity (GHSV) = 5000 h^{-1} and steam-to-carbon ratio (S/C) = 6.5. These working conditions are not practical because of the high S/C ratio and low hydrogen production rate [15]. Co/CeO₂ catalysts also show good resistance to carbon deposition during ESR, which has attracted much attention recently [16-18]. It was found that Co/CeO₂ catalysts prepared by different methods showed significant differences in ESR activity. Song et al. [18] prepared Co/CeO₂ catalysts using three different methods: solvothermal method, colloidal crystal templating, and reverse microemulsion. These catalysts gave much better performance than those prepared by incipient wetness impregnation. The superiority of these preparation methods was attributed to a better cobalt dispersion and enhanced metal-oxide interaction. However, these preparation methods are too complex and not practical. The citric acid complexing method is a cost effective preparation method for uniform composite oxide formation at relatively low temperatures. It gives a high yield with a simple equipment setup [19]. Catalysts prepared by this method have been applied to the partial oxidation of methane and ESR [20,21]. The present work prepared Co/CeO₂ catalysts by citric acid complexing. The effect of calcium doping was also investigated. In view of a recently developed membrane reformer

for ESR [22–25], ESR was investigated in the temperature range of 450–650 °C at a practical GHSV.

1 Experimental

1.1 Catalyst preparation

The catalysts were prepared by the citric acid complexing method. Nitrates of cobalt, cerium, and calcium purchased from Sinopharm Chemical Reagent Co. Ltd. were utilized as starting materials without purification. A mixed solution of the nitrates with a total cation concentration of 1.0 mol/L was prepared by dissolving the nitrates in deionized water. Citric acid was added as a complexing agent in a molar ratio of 2:1. After complete mixing and stirring at 60 °C, a transparent solution was obtained. Then most of the water was evaporated at 80 °C to give a sol. A viscous gel was obtained after further stirring and evaporation. After drying at 120 °C overnight, the resulting spongy solid was heated in air in a muffle furnace from room temperature to 600 °C with a temperature ramp rate of 5 °C/min and kept at 600 °C for 4.0 h.

1.2 Catalyst characterization

The specific surface area, pore volume, and pore size distribution were characterized by N_2 adsorption at liquid nitrogen temperature using a Quantachrome NOVA 2200E. Prior to adsorption, the samples were degassed at 350 °C for 2.0 h to remove physically adsorbed components. The surface area was determined from the linear portion of the Brunauer-Emmett-Teller (BET) equation. Pore volume and pore size distribution were calculated by the Barrett-Joiner-Halenda (BJH) method using the desorption branch of the isotherm.

Temperature programmed reduction (TPR) experiments were conducted on a microreactor-gas chromatograph (GC) system using a 5% H₂-95% Ar atmosphere. The sample (50.0 mg) was heated from room temperature to 400 °C under 30.0 ml/min Ar flow and kept at 400 °C for at least 30 min, and then cooled down to room temperature. The Ar was switched to 30.0 ml/min 5% H₂-95% Ar gas, and the sample was heated with a linear temperature rise from 100 to 900 °C at a rate of 10 °C/min. Hydrogen consumption was measured online with a thermal conductivity detector (TCD).

X-ray powder diffraction (XRD) was used to determine the phase composition and size of the catalysts before and after reduction. The XRD measurements were performed on a Rigaku D/MAX2500VL/PC apparatus using nickel filtered Cu K_{α} radiation ($\lambda = 0.1541$ nm), operating voltage of 40 kV and current of 40 mA. The crystallite sizes of the particles were measured using the peak width at half peak height and the Debye-Scherrer equation.

FT-IR spectra were recorded using a Perkin-Elmer Spectrum 100 spectrometer equipped with a deuterated triglycine sulfate detector. The spectra were collected at a resolution of 4.0 cm⁻¹ using 32 scans in the range of 400–4000 cm⁻¹. All the samples were prepared as KBr pellets.

High resolution transmission microscopy (HR-TEM) was recorded using a JEOL-2100 microscope. TEM were prepared by the ultrasonic dispersion of slightly ground catalyst samples in ethanol, and then a drop of the suspension was applied onto a holey carbon grid.

1.3 Catalytic activity test

Catalytic activity was measured using a fixed bed reactor of stainless steel with an inner diameter of 8.0 mm. The catalyst (200 mg) of 60-80 mesh grain size were diluted with quartz sand and loaded into the reactor to achieve a catalyst bed height of 5.0 mm. A K-type thermocouple inserted into the center of the catalyst bed was used to detect the temperature. Prior to reaction, catalysts were heated at 10 °C/min in 5% H₂-95% Ar flow at 30.0 ml/min from room temperature to 450 or 650 °C and kept at 450 or 650 °C for 2.0 h. Then, ethanol, water and N₂ gas were delivered to the reactor. The reaction products were monitored by an online GC equipped with TCD and flame ionization detectors (FID). N₂ was used as the internal standard for calculations as well as a dilution gas. CH₄ showed signals in both the TCD and FID detectors, thus the analysis of all products was obtained. Data with a carbon balance over 95% were used. Ethanol conversion was calculated by

 $X_{\text{ethanol}} = (F_{\text{ethanol,in}} - F_{\text{ethanol,out}})/F_{\text{ethanol,in}} \times 100\%$ (9) The yield of hydrogen was defined as the ratio between hydrogen generated (moles) and six times the ethanol fed (moles) and calculated by

 $Y_{\text{hydrogen}} = \text{moles of H}_2 \text{ produced/(6 } \times \text{ moles of ethanol fed}) \\ \times 100\%$ (10)

The selectivity of carbon-containing products was calculated by

$$S_{C_xH_yO_z} = i F_{C_xH_yO_z} / (2F_{\text{ethanol,in}}) \times 100\%$$
(11)

where $F_{\text{ethanol,in}}$ was the flow of ethanol in the gas phase at the inlet of the reactor and $F_{\text{ethanol,out}}$ was the flow of ethanol in the gas phase at the outlet of the reactor. $F_{\text{ethanol,in}}$ was calculated from the liquid ethanol fed rate, and $F_{\text{ethanol,out}}$ was calculated using the GC analysis results and the standard gas feed rate. $C_xH_yO_z$ represents carbon-containing products such as CH₄, CO, and CO₂, and possible other products. The steam-to-carbon ratio was the molar ratio of the steam and carbon (each mole ethanol correspond to two moles carbon) flow rates at the inlet of the reactor.

2 Results and discussion

2.1 Characterization

Table 1 shows the BET specific surface area, pore volumes, and average pore sizes of the catalysts. The surface areas were not high, and the pore volumes were in the range of 0.09–0.14 ml/g. The pore sizes were in the range of 7.4–10.1 nm. The low surface areas were due to the combustion reaction between the metal nitrates and citric acid during calcination, which gave a high temperature and sintering of the composite oxides.

Catalyst [*]	Surface area	Pore volume	Average pore size
	(m^2/g)	(ml/g)	(nm)
$Co_{0.1}Ce_{0.9}O_y$	8.7	0.09	10.1
$Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$	19.4	0.12	8.5
$Co_{0.1}Ce_{0.8}Ca_{0.1}O_y$	18.2	0.11	7.8
$Co_{0.1}Ce_{0.75}Ca_{0.15}O_y$	20.3	0.14	7.4

*Mass ratio of atom in samples.

Figure 1 shows the XRD patterns of the Co/CeO₂ catalysts. Cubic CeO₂ was the main phase. Co₃O₄ was not clearly seen and the CaO phase was not detected by XRD, suggesting its probable high dispersion on the surface of CeO₂. Compared with pure CeO₂, the intensity of the XRD peaks for CeO₂ in the catalysts was smaller and the width of the peaks for CeO2 broader, indicating that cobalt and calcium doping resulted in the formation of CeO₂ with a smaller particle size. From the Scherrer equation, the CeO₂ particle $Co_{0.1}Ce_{0.9}O_{y}$, $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$, sizes in Co_{0.1}Ce_{0.8}Ca_{0.1}O_v, and Co_{0.1}Ce_{0.75}Ca_{0.15}O_v were 18.3, 14.7, 13.6, and 10.4 nm, respectively. The Co₃O₄ cubic phase was not as clearly shown as compared with catalysts prepared by incipient wetness impregnation [16], showing that the Co₃O₄ phase was finely dispersed. After reduction at 650 °C for 2.0 h, the CeO₂ particle size, deduced from the XRD characterization, for $Co_{0.1}Ce_{0.9}O_{\nu}$, $Co_{0.1}Ce_{0.85}Ca_{0.05}O_{\nu}$, Co_{0.1}Ce_{0.8}Ca_{0.1}O_v, and Co_{0.1}Ce_{0.75}Ca_{0.15}O_v were 21.5, 15.8, 15.1, and 12.2 nm, respectively. The average particle sizes cobalt of in $Co_{0.1}Ce_{0.9}O_{v}$, $Co_{0.1}Ce_{0.85}Ca_{0.05}O_{\nu}$ $Co_{0.1}Ce_{0.8}Ca_{0.1}O_{\nu}$, and $Co_{0.1}Ce_{0.75}Ca_{0.15}O_{\nu}$ calculated from the Scherrer equation were 12.8, 13.1, 13.4, and 14.2 nm, respectively, which agreed with the HR-TEM characterization results in Fig. 2.

HR-TEM characterization results are shown in Fig. 2, which also suggested the nano-structure of the CeO_2 support as well as the nanostructure of Co^0 . The average particle



Fig. 1. XRD patterns of Co/CeO₂ catalysts after calcination (a) and after reduction at 650 °C (b). (1) $Co_{0.1}Ce_{0.9}O_{y}$; (2) $Co_{0.1}Ce_{0.85}Ca_{0.05}O_{y}$; (3) $Co_{0.1}Ce_{0.8}Ca_{0.1}O_{y}$; (4) $Co_{0.1}Ce_{0.75}Ca_{0.15}O_{y}$.



Fig. 2. TEM images of $Ce_{0.9}Co_{0.1}O_y$ after reduction (a, d), used $Ce_{0.9}Co_{0.1}O_y$ (b, e), and used $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$ (c, f) catalysts.

size of Co^0 (dark part) in $\text{Co}_{0.1}\text{Ce}_{0.9}\text{O}_y$ after reduction was 14.0 nm, while the particle sizes of CeO_2 were in the range of 13.0–30.0 nm. The TEM characterization also suggested that 5% calcium doping had an obvious influence on ceria particle size, but little effect on cobalt particle size.

Figure 3 shows FT-IR spectra for $Co_{0.1}Ce_{0.9}O_y$, $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$, $Co_{0.1}Ce_{0.8}Ca_{0.1}O_y$, and $Co_{0.1}Ce_{0.75}Ca_{0.15}O_y$ in the wave number range of 500–4000 cm⁻¹. The FT-IR characterization gave information on two problems. The first was the effect of calcium addition into Co/CeO₂ on carbonate formation. Figure 3(a) clearly indicated that too much calcium (15.0 wt%) addition caused much carbonate formation, which was shown by the FT-IR peaks at 1419 and 870 cm⁻¹. Thus, it was deduced that too much calcium doping would cause acetate formation during ESR, which is believed to be one of the reasons for catalyst deactivation [28].

Figure 3(b) shows the IR region in which superoxide O_2^{-1} was detected. Oxygen storage begins with the activation of gaseous O2 molecules on O vacancies associated with reduced cerium sites (Ce³⁺), known as coordinatively unsaturated sites (CUS) on the surface of the composite oxide [29,30]. This activation results in the formation of O radicals upon exposure of the surface to O_2 , due to the reduction of O₂ and subsequently oxidation of the Ce³⁺ CUS. Among the various O radicals that can be progressively formed, the O_2^- is very stable and it is considered a key species or an oxygen storage initiator for both surface and bulk storage [29,30]. O₂⁻ radicals can be detected by FT-IR [31]. The band at 1121 cm⁻¹ was assigned to the superoxide species. This band was observed with $Co_{0.1}Ce_{0.9}O_{\nu}$ and $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$, but not with $Co_{0.1}Ce_{0.8}Ca_{0.1}O_y$ and Co_{0.1}Ce_{0.75}Ca_{0.15}O_v. The results indicated that too much calcium doping into Co/CeO₂ through citric acid complexing



Fig. 3. FT-IR characterization of Co/CeO₂ with and without calcium doping. (a) FT-IR spectra in the range 500–4000 cm⁻¹; (b) IR spectra of O_2^- in the range 1080–1180 cm⁻¹. (1) Co_{0.1}Ce_{0.9}O_y; (2) Co_{0.1}Ca_{0.05}Ce_{0.85}O_y; (3) Co_{0.1}Ca_{0.0}Ce_{0.8}O_y; (4) Co_{0.1}Ca_{0.15}Ce_{0.75}O_y.

deteriorated its oxygen storage capacity, which is detrimental to surface oxygen reduction. As the formation of the Ce^{3+} -O-Co⁰ metal-oxide interface has been proposed as necessary for the active sites for ESR by Chen [26] and de Lima [27], thus the ESR catalytic performance was affected by the particle size of the cobalt and ceria, as well as the reduction degree of Ce⁴⁺. Calcium doping hindered the sintering of the ceria support by its isolation of small ceria particles during calcination, but it also affected Ce³⁺-O-Co⁰ metal-oxide interface formation and ESR catalytic performance.

Figure 4 shows the H₂-TPR spectra for Co_3O_4 , CeO_2 , $Co_{0.1}Ce_{0.9}O_y$, $Co_{0.1}Ce_{0.8}Ca_{0.1}O_y$, $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$, and $Co_{0.1}Ce_{0.75}Ca_{0.15}O_y$. The overlapping peak in Fig. 4 after Gaussian deconvolution suggested that Co_3O_4 reduction



Fig. 4. H₂-TPR profiles of Co/CeO₂ catalysts with and without calcium doping. (1) Co_3O_4 ; (2) CeO_2 ; (3) $Co_{0.1}Ce_{0.9}O_y$; (4) $Co_{0.1}Ca_{0.05}Ce_{0.85}O_y$; (5) $Co_{0.1}Ca_{0.1}Ce_{0.8}O_y$; (6) $Co_{0.1}Ca_{0.15}Ce_{0.75}O_y$.

proceeded by two steps: first the reduction of Co^{3+} to Co^{2+} and then of Co^{2+} to Co^{0-} . The first reduction peak temperature at 320 °C was assigned to the reduction of Co^{3+} to Co^{2+} and the second at 380 °C was attributed to Co2+ reduction to Co^{0} . With ceria, two reduction peaks were observed. The first broad peak at 400 °C was attributed to the reduction of surface and subsurface Ce^{4+} to Ce^{3+} , and the second peak at 800 °C was due to the reduction of bulk Ce⁴⁺. For $Co_{0.1}Ce_{0.9}O_{\nu}$, the interaction of Co_3O_4 and CeO_2 benefited the reduction of Co^{3+} to Co^{2+} and Ce^{4+} to Ce^{3+} . During Co_3O_4 reduction of $Co_{0,1}Ce_{0,9}O_{\nu}$, the peak temperature for Co³⁺ reduction to Co²⁺ was decreased from 322 to 304 °C. For some of the surface Co_3O_4 , the reduction temperature was as low as 250 °C. The peak temperature for Co²⁺ reduction to Co⁰ was decreased from 382 to 354 °C, suggesting a close interaction between Co₃O₄ and CeO₂. Calcium doping of the catalysts would increase their sintering resistance during the ESR reaction. However, it was detrimental for Co₃O₄ and CeO₂ reduction and Ce³⁺-O-Co⁰ formation. Calcium doping hindered the interaction between Co₃O₄ and CeO_2 to some extent, which was shown in the H₂-TPR characterization results. Calcium (5.0%) doping increased the peak temperature for Co^{3+} reduction to Co^{2+} from 304 to 352 °C, and Co²⁺ reduction to Co⁰ from 354 to 424 °C. With the increase of calcium doping content, the reduction temperature shifted to higher temperatures, indicating that calcium doping weakened the interaction between Co₃O₄ and CeO₂. These results are not in agreement with the findings by Song et al. [32] who doped 5.0% calcium into CeO₂ by coprecipitation, and then prepared calcium doped Co/CeO2 by incipient wetness impregnation. They found that 5% calcium doping of the catalysts benefited the reduction of Co₃O₄ as well as CeO₂. This significant difference was attributed to the preparation methods. In the impregnation method, Co₃O₄ is supported on the surface of CeO₂, and calcium doping mainly influenced the properties of CeO₂, but had little effect on the interaction between Co₃O₄ and CeO_2 . For the Co/CeO₂ catalysts prepared by citric acid complexing, calcium doping was shown to influence the interaction between CeO₂ and Co₃O₄ by FT-IR and TEM characterization. Moreover, calcium doping also hindered the promoting effect of Co₃O₄ on CeO₂ reduction, as shown by the TPR characterization in which the peak temperature for bulk CeO₂ reduction increased from 591 to 676 °C when the calcium content increased from 5.0% to 15.0%.

2.2 Catalytic performance

The influence of pre-reduction temperature on catalytic performance was investigated. Two temperatures, 450 and 650 °C, were chosen from the H₂-TPR characterization results. The two temperatures were chosen according to the following consideration. Co_3O_4 and surface CeO_2 can be reduced at 450 °C, while Co_3O_4 , surface and some bulk CeO_2 can be reduced at 650 °C. The catalytic performance of $Co_{0.1}Ce_{0.9}O_y$, $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$, $Co_{0.1}Ce_{0.8}Ca_{0.1}O_y$, and $Co_{0.1}Ce_{0.75}$ -Ca_{0.15} O_y activated at 450 °C gave better performance in terms of ethanol conversion. For example, with $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$ catalyst activated at 450 °C, ethanol was not efficiently converted at 400 °C, while with $Co_{0.1}Ce_{0.9}O_y$.

catalyst activated at 650 °C, ethanol conversion reached 40.5% at 400 °C. Similar trends were observed for the $Co_{0.1}Ce_{0.9}O_y$, $Co_{0.1}Ce_{0.8}Ca_{0.1}O_y$, and $Co_{0.1}Ce_{0.75}Ca_{0.15}O_y$ catalysts, with much higher ethanol conversions from catalysts activated at 650 °C than from those activated at 450 °C when the reaction temperature was in the range of 400–500 °C. However, when the reaction temperature was over 550 °C, ethanol conversion was not very different for catalysts activated at 450 and 650 °C. The result is related to in situ reduction of the catalysts under working conditions. The hydrogen content in the reformate increased with ethanol conversion, and the in situ generated hydrogen can be utilized as a reduction agent for catalyst reduction.

The catalytic performance of the catalysts confirmed the FT-IR and H₂-TPR characterization results, which suggested that > 5% calcium doping resulted in deteriorated oxygen storage capacity. The oxygen storage capacity of Co/CeO₂ has a significant effect on ESR according to the reaction mechanism proposed by de Lima [27]. The diffuse reflection infrared Fourier transform spectroscopy (DRIFTS) characterization of ethanol desorption and DRIFTS under reaction conditions showed a junction effect between metal and support. Ethoxy species were generated on the surface of partially reduced ceria by dissociative adsorption. Oxidative dehydrogenation occurred with surface -OH on the support to form an acetate intermediate, liberating H₂ in the process at the support-metal interface [33]. During oxidation and oxidative steam reforming, the dehydrogenated species can react with oxygen species from the support to produce acetate species. In the presence of co-adsorbed steam, the acetate decomposition reaction is favored, generating CO_x and CH_x. Calcium doping decreased the catalytic activity, although the particle size of ceria CeO₂ was decreased and that of Co⁰ was not changed. The decreased catalytic performance was probably due to CaO fouling of CeO_2 and the smaller Ce^{3+} -Co interface [34].



Fig. 5. Catalytic performance for catalysts activated at 450 °C (1) and 650 °C (2) for ethanol steam reforming. (a) $Co_{0.1}Ce_{0.9}O_{y}$; (b) $Co_{0.1}Ca_{0.05}Ce_{0.85}O_{y}$; (c) $Co_{0.1}Ca_{0.1}Ca_{0.1}Ce_{0.8}O_{y}$; (d) $Co_{0.1}Ca_{0.15}Ce_{0.75}O_{y}$. Reaction conditions: GHSV = 50000 ml/(g·h), C_2H_5OH :water: N_2 = 1:6:18, p = 101 kPa.



Fig. 6. Selectivity and hydrogen yield over different catalysts reduced at 650 °C. (a) Hydrogen yield; (b) CH₄ selectivity; (c) CO₂ selectivity; (d) CO selectivity. (1) $Co_{0.1}Ce_{0.9}O_y$; (2) $Co_{0.1}Ca_{0.05}Ce_{0.85}O_y$; (3) $Co_{0.1}Ca_{0.1}Ce_{0.8}O_y$; (4) $Co_{0.1}Ca_{0.15}Ce_{0.75}O_y$. Reaction conditions: GHSV = 50000 ml/(g·h), C_2H_5OH :water: $N_2 = 16:18$, p = 101 kPa.

Figure 6 shows the selectivity to CO₂, CO, CH₄, and hydrogen for $Co_{0,1}Ce_{0,9}O_{\nu}$ $Co_{0,1}Ce_{0,85}Ca_{0,05}O_{\nu}$ Co_{0.1}Ce_{0.8}Ca_{0.1}O_v, and Co_{0.1}Ce_{0.75}Ca_{0.15}O_v catalysts reduced at 650 °C. At low temperatures, ethanol was not completely converted into C1 species. CH3CHO and CH3COCH3 were observed in products. With increasing reaction temperature to over 450 °C, there was no CH₃CHO and CH₃COCH₃ in the product, and ethanol was completely converted into C₁ species. The product distribution was kinetically controlled and depended on reaction temperature and catalyst. During ESR, water gas shift (WGS) and methanation also occurred. To get a good hydrogen yield, a catalyst with good activity for both the ESR and WGS reactions is desired. The Co_{0.1}Ce_{0.9}O_v catalyst showed high WGS activity, and the highest selectivities for CO₂ were obtained at temperatures below 550 °C. However, at 600 and 650 °C, the selectivities for CO₂ over the Co_{0.1}Ce_{0.9}O_v catalyst was slightly lower than those over the other catalysts, which were attributed to the higher activity for the WGS and also reverse WGS reactions of the $Co_{0.1}Ce_{0.9}O_{\nu}$ catalyst. Thus, the selectivity for CO_2 over $Co_{0.1}Ce_{0.9}O_{\nu}$ was thermodynamically controlled,

while over the other catalysts, it was kinetically controlled. The selectivity for CH₄ was also found to depend on the catalyst and reaction temperature. At 500 °C, a lower selectivity for CH₄ was obtained with all the catalysts. According to Eq. (6), each mole of CH₄ formation consumes three moles hydrogen, and a lower selectivity for CH₄ would give a higher hydrogen yield. CH₄ formation proceeds through two routes: ethanol direct decomposition and methanation. At low reaction temperature, ethanol direct decomposition dominates. However, at high temperatures, CH₄ steam reforming instead of methanation dominates. The selectivity for CH₄ was closely related with methane steam reforming and ethanol decomposition. Hydrogen yields over the different catalysts are also shown in Fig. 6(a). Over the $Co_{0.1}Ce_{0.9}O_{\nu}$ catalyst, a hydrogen yield of 89.2% was obtained at 500 °C. The selectivities for CH₄, CO, and CO₂ were 6.0%, 8.5%, and 85.5%, respectively. At lower temperatures, side products such as acetaldehyde and acetone decreased the hydrogen yield, and less than 50% hydrogen yield were obtained. A high reaction temperature also decreased hydrogen yield due to a higher selectivity for CO. A

temperature around 500 °C was the best, where hydrogen yields over 85% were obtained over all the catalysts. On comparing the hydrogen yield over different catalysts, it can be concluded that calcium doping significantly decreased hydrogen yield below 500 °C due to its hindrance effect on the interaction between CeO₂ and Co₃O₄ and a lower oxygen storage capacity. However, at temperatures above 550 °C, slightly higher hydrogen yields were obtained over the doped catalysts, which can be attributed to the slightly lower selectivity for CO, as shown in Fig. 6.

As shown by the characterization, activation, and catalytic performance of the catalysts, the catalysts for ESR should have small crystallites of the metallic cobalt active phase and easily reducible and accessible Ce³⁺ for steam adsorption. On the surface of metallic cobalt, activation of ethanol occurs, while over partially reduced ceria, activation of water occurred. The close contact of both components and a short enough distance from the boundary to the center of the surface of cobalt crystallites have a significant influence on ESR. The reagents and reaction intermediates chemisorbed on cobalt and on the ceria support have to interact to form the desired products of ESR: hydrogen and carbon dioxide. If the distance from the cobalt-support boundary is too large (it is the case with large cobalt crystallites) and since water is not strongly activated on the support, a non-selective transformation of ethanol takes place without the possibility that the by-products or intermediates can react with activated water from the support. Under this circumstance, it is possible to obtain 100% ethanol conversion to acetaldehyde as the primary product over the cobalt surface. Due to a low surface concentration of activated water adsorbed on the support near the cobalt-support border, much acetaldehyde remains in the final product. There is no further reaction of acetaldehyde with water to form the desired products (CH₃CHO + H₂O \rightarrow 3H₂ + 2CO or

CH₃CHO + 3H₂O → 5H₂ + 2CO₂). Similarly, for the same reason, acetone remains in the product. Large crystallites of cobalt, a large distance from the cobalt-support boundary to the center, low concentration of activated water on the support, and the chemical nature of the support result in a low rate of WGS. Carbon monoxide can be formed on the cobalt active phase by the direct decomposition of ethanol (eq. 2) or acetaldehyde (CH₃CHO → CO + CH₄) and by the steam reforming of ethanol and acetaldehyde (C₂H₅OH + H₂O → 2CO + 4H₂, CH₃CHO + H₂O → 3H₂ + 2CO) when the water concentration is insufficient [35–37]. A small contribution of the WGS reaction to the ESR pathway on these catalysts results also in low selectivities towards hydrogen and carbon dioxide when compared with thermodynamic values.

2.3 Stability

The stabilities of the $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$ and $Co_{0.1}Ce_{0.9}O_y$ catalysts were investigated. The results are shown in Fig. 7. During 50.0 h on stream, the ethanol conversion was maintained at almost 100%, and hydrogen selectivity of 85%, and selectivities for CH₄, CO, and CO₂ of 8.0%, 16.0%, and 76.0% were maintained. TEM characterization of reduced Co_{0.1}Ce_{0.85}Ca_{0.05}O_v and the used catalyst showed no obvious sintering of cobalt and ceria in the Co_{0.1}Ce_{0.85}Ca_{0.05}O_y catalyst. The good stability was closely related to the working conditions as well as the catalyst itself. A S/C of 3.0 prevents carbon deposition. HRTEM characterization of the used catalysts also showed that no carbon deposition occurred. The weak basic property of the catalyst efficiently prevented ethanol dehydration to ethylene, which is believed to be a carbon deposition source. Although both the $Co_{0.1}Ce_{0.9}O_{\nu}$ and $Co_{0.1}Ce_{0.85}Ca_{0.05}O_{\nu}$ catalysts maintained their activity and product selectivities during 50.0 h on



Fig. 7. Stability test of $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$ (a) and $Co_{0.1}Ce_{0.9}O_y$ (b) catalysts. Reaction conditions: T = 550 °C, S/C = 3.0, GHSV = 50000 ml/(g·h), $C_2H_5OH:H_2O:N_2 = 1:6:18$, p = 101 kPa. (1) Ethanol conversion; (2) H_2 selectivity; (3) CO₂ selectivity; (4) CO selectivity; (5) CH₄ selectivity.

stream, TEM images of the used $Co_{0.1}Ce_{0.9}O_y$ and $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$ catalysts (shown in Fig. 2) indicated that whisker carbon deposition has occurred on the $Co_{0.1}Ce_{0.9}O_y$ catalyst, while this not seen on the $Co_{0.1}Ce_{0.85}Ca_{0.05}O_y$. Calcium doping increased the resistance to carbon deposition of the catalyst, which was attributed to the small particle size of ceria and basicity of CaO.

3 Conclusions

A Co/CeO₂ catalyst and Co/CeO₂ catalysts modified with 5.0%, 10.0%, and 15.0% calcium doping were prepared by the citric acid complexing method. The catalysts showed good activity for ethanol steam reforming, with 100% ethanol conversion into C1 species at reaction temperatures over 500 °C at a GHSV = 50000 ml/($g\cdot h$), S/C = 3.0, and atmospheric pressure. The hydrogen yield was as high as 90% under optimized conditions. Calcium doping in the Co/CeO₂ catalysts reduced the ceria particle size but made them more difficult to reduce, which deteriorated oxygen storage capacity and catalytic performance when the calcium content was over 5.0%. The poorer catalytic performance was probably because of a smaller Co⁰-O-Ce³⁺ metal-oxide interface due to CaO fouling of CeO2. Stability investigation of the Co_{0.1}Ce_{0.9}Oy and Co_{0.1}Ce_{0.85}Ca_{0.05}Oy catalysts suggested that the small particle size of ceria and weak basic property of the catalyst gave better carbon deposition resistance. Activity measurement results from catalysts pre-reduced at different temperatures suggested that Ce³⁺ formation was needed for ethanol steam reforming.

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